

# Guidelines on Methodologies for Source Emission Monitoring



**Central Pollution Control Board  
Ministry of Environment and Forests**

Website: [www.cpcb.nic.in](http://www.cpcb.nic.in)

Laboratory Analytical Techniques  
Series: LATS / 80 / 2013-2014

# GUIDELINES ON METHODOLOGIES FOR SOURCE EMISSION MONITORING



**Central Pollution Control Board**  
(Ministry of Environment & Forests)  
Parivesh Bhawan, East Arjun Nagar, Delhi - 110 032  
Website: [www.cpcb.nic.in](http://www.cpcb.nic.in)



CPCB, 200 Copies, 2012

---

*Prepared & Published by* P R Division, Central Pollution Control Board on behalf of  
Sh. J. S. Kamyotra, Member Secretary, CPCB

*Printing Supervision:-* Shri G. Ganesh, Ms Anamika Sagar and Shri Satish Kumar

*Printed at :-* Aravali Printer & Publishers Pvt. Ltd.



मीरा महर्षि

अध्यक्ष

**MIRA MEHRISHI**

Chairman

**केन्द्रीय प्रदूषण नियंत्रण बोर्ड**

(भारत सरकार का संगठन)

पर्यावरण एवं वन मंत्रालय

**Central Pollution Control Board**

(A Govt. of India Organisation)

Ministry of Environment & Forests

Phone : 22304948/22307233

## FOREWORD

To harmonize the methodologies adopted by the State Pollution Control Boards/ Pollution Control Committees, Central Pollution Control Board has taken up the task to collate and compile the techno-feasible and internationally compatible source emission monitoring methodologies for all the criteria pollutants (PM, SO<sub>2</sub>, NO<sub>x</sub>) and including special parameters like HCl, HF. This exercise has been an ongoing activity of CPCB catering to the continuous need of standard development and harmonizing protocols for emission measurements being done by regulatory authorities. The first effort was made by CPCB in 1985 with the publication of Emission Regulation (Part III) - a document on Isokinetic sampling of Particulate Matter. The present document is an updated version based on enhanced need with the inclusion of new parameters in emission regulation.

The effort of Shri Abhijit Pathak, 'B', air Laboratory in compilation and collation of information is appreciated. The exercise was possible under the encouraging supervision of Dr. D. Saha, Scientist 'D' and the guidance of Shri J.S. Kamyotra, Member Secretary, CPCB.

I trust and believe that the SPCBs / PCCs, industries and other stakeholders will find this document useful for improving their technical competence to adjudge industrial compliance status.

August, 2012

**MIRA MEHRISHI**  
Chairman CPCB

---

'Parivesh Bhawan' C.B.D-cum Office Complex, East Arjun Nagar, Delhi-110 032  
Fax : 22304948 / 22307078 e-mail : ccb.cpcb@nic.in Website : <http://www.cpcb.nic.in>

# CONTENTS

|                    |  |              |
|--------------------|--|--------------|
| <b>Chapter – 1</b> | <b>Material and Methodology for Isokinetic Sampling</b>                        | <b>1-25</b>  |
| <b>Part I</b>      |  | <b>1-18</b>  |
| 1.0                | Source Emission Monitoring   | 1            |
| 2.0                | References   | 18           |
| <b>Chapter – 1</b> | <b>Determination of particulate matter emissions</b>                           |              |
| <b>Part II</b>     |  | <b>19-25</b> |
| 1.0                | Principle  | 19           |
| 2.0                | Applicability  | 19           |
| 3.0                | Interferences  | 19           |
| 4.0                | Sampling   | 19           |
| 5.0                | Procedure for Particulate Matter Determination                                 | 19           |
| 6.0                | Sample Recovery  | 22           |
| 7.0                | Calculation  | 22           |
| 8.0                | References   | 25           |
| <b>Chapter – 2</b> | <b>Standard Operating Procedure for Determination of Particulate Matter</b>    | <b>26-34</b> |
| 1.0                | Pre Sampling Activity  | 26           |
| 2.0                | Traverse Point Calculation   | 26           |
| 3.0                | Determination of Composition of Flue Gas                                       | 26           |
| 4.0                | Measure ambient temperature (°C) and Barometric pressure in mm Hg              | 26           |
| 5.0                | Check the Leak in Sampling Train   | 26           |
| 6.0                | Moisture Determination   | 27           |
| 7.0                | Wet Molecular Weight Determination   | 27           |
| 8.0                | Determine Stack Gas Velocity Pressure( $\Delta P$ ) And Stack Temperature (Ts) | 28           |
| 9.0                | Determination Of Static Pressure (Absolute Stack Gas Pressure)                 | 28           |
| 10.0               | Stack Gas Velocity Determination (Us)  | 28           |
| 11.0               | Determination of Volumetric Flow Rate/ Discharge                               | 29           |
| 12.0               | Determination of Flow at Nozzle  | 29           |
| 13.0               | Determination of Sampling Rate at the Gas Meter                                | 30           |
| 14.0               | Sampling   | 30           |
| 15.0               | Determination of Volume of Gas Sampled   | 31           |
| 16.0               | Sample Recovery  | 31           |

|                    |   |              |
|--------------------|---|--------------|
| 17.0               | Determination of Dust Concentration   | 31           |
| 18.0               | Correction of the result at 11 % Oxygen   | 32           |
| 19.0               | Determination of Emission Rate  | 32           |
| <b>Chapter – 3</b> | <b>Determination of Hydrogen Halides (Hx) and Halogens in Emission</b>            | <b>35-48</b> |
| <b>Part (i)</b>    | <b>Sampling of Hydrogen Halides(Hx) and Halogens</b>                              | <b>35-40</b> |
| 1.0                | Principle   | 35           |
| 2.0                | Applicability   | 35           |
| 3.0                | Interferences   | 35           |
| 4.0                | Reagents  | 36           |
| 5.0                | Sampling  | 36           |
| 6.0                | Sample Analysis   | 39           |
| 7.0                | Calculation   | 39           |
| <b>Part (ii)</b>   | <b>Analysis of Hx and Halogens</b>  | <b>41-48</b> |
| 1.0                | Purpose and Applicability   | 41           |
| 2.0                | Summary of Method   | 41           |
| 3.0                | Interferences   | 41           |
| 4.0                | Apparatus and Materials   | 41           |
| 5.0                | Sample Handling   | 43           |
| 6.0                | Calculation and Data Reduction  | 45           |
| 7.0                | Quality Assurance and Quality Control   | 46           |
| 8.0                | References  | 47           |
| <b>Chapter – 4</b> | <b>Standard Operating Procedure for Sampling of Hydrogen Halides and Halogens</b> | <b>49-53</b> |
| 1.0                | Purpose and Applicability   | 49           |
| 2.0                | Pre Sampling Activities   | 49           |
| 3.0                | Preparation of Reagents   | 49           |
| 4.0                | Field Activities and Isokinetic Sampling  | 50           |
| 5.0                | Preparation of the Sampling Train   | 50           |
| 6.0                | Sample Collection   | 50           |
| 7.0                | Sample Recovery   | 51           |
| <b>Chapter – 5</b> | <b>Determination of Metals and Non Metals in Emissions</b>                        | <b>54-69</b> |
| 1.0                | Principle   | 54           |
| 2.0                | Applicability   | 54           |
| 3.0                | Interferences   | 55           |
| 4.0                | Reagents  | 56           |



|                    |  |               |
|--------------------|--|---------------|
| 5.0                | Procedure  | 58            |
| 6.0                | Calculation  | 64            |
| 7.0                | References   | 69            |
| <b>Chapter – 6</b> | <b>Standard Operating Procedure (SOP) for Sampling, Sample Preparation and Analysis of Metals and Non Metals</b> | <b>70-84</b>  |
| <b>Part I</b>      | <b>Standard Operating Procedure (SOP) for Sampling</b>   | <b>71-80</b>  |
| 1.0                | Purpose and Applicability  | 71            |
| 2.0                | Pre-sampling Activities  | 72            |
| 3.0                | Preparation of Reagents  | 72            |
| 4.0                | Preparation of sampling train  | 73            |
| 5.0                | Field Activity   | 74            |
| 6.0                | Sample Recovery  | 74            |
| <b>Part II</b>     | <b>Standard Operating Procedure (SOP) of Sample Preparation and analysis</b>                                     | <b>81-84</b>  |
| 1.0                | Sample Preparation   | 81            |
| 2.0                | Sample Digestion / Extraction  | 81            |
| 3.0                | Sample Analysis  | 83            |
| 4.0                | Calculation  | 83            |
| <b>Chapter – 7</b> | <b>Determination of Sulfur Dioxide in Emissions</b>  | <b>85-95</b>  |
| 1.0                | Principle and Applicability  | 85            |
| 2.0                | Apparatus  | 85            |
| 3.0                | Reagents   | 89            |
| 4.0                | Procedure  | 90            |
| 5.0                | Calibration  | 92            |
| 6.0                | Calculation  | 93            |
| 7.0                | Bibliography   | 95            |
| <b>Chapter – 8</b> | <b>Determination of Nitrogen Oxides in Emissions</b>   | <b>96-106</b> |
| 1.0                | Principle and Applicability  | 96            |
| 2.0                | Apparatus  | 96            |
| 3.0                | Reagents   | 99            |
| 4.0                | Procedure  | 101           |
| 5.0                | Calibration  | 103           |
| 6.0                | Calculation  | 105           |
| 7.0                | Bibliography   | 106           |

## Method-1 (Part- I)

### Stack Monitoring – Material and Methodology for Isokinetic Sampling

#### 1.0 SOURCE EMISSION MONITORING

This section deals with the method of source emission monitoring. It also gives the minimum requirement of a stack monitoring equipment.

#### 1.1 Specifications of Stack Monitoring Equipment

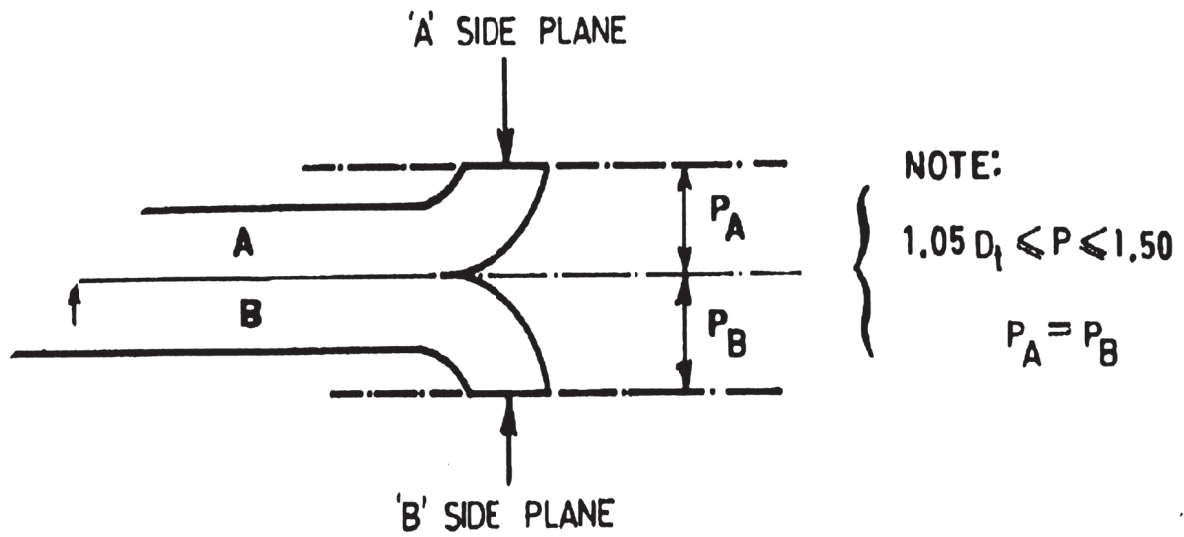
**Table 1.1: Specifications of Stack Monitoring Equipment**

| S.N.                        | Item/Equipment  | Specifications / Applicable ranges   |
|-----------------------------|---|--|
| <b>General Requirements</b> |   |  |
| 1                           | Stack Velocity Range:<br><br>Stack Temperature:<br>Range Particulate<br>Sampling:<br>Filter Paper (Thimble):<br>Gaseous sampling: | 0 to 30 m /sec<br><i>For low velocity range differential pressure determination should be done by differential manometer</i><br>0 to 600 °C)<br>At 10 to 60 lpm<br>Collection of particulates down to 0.3 micron<br>At 1 to 2 LPM collection on a set of impingers containing selective reagents.  |
| 2                           | Pitot tube  | i. Pitot tube shall be modified “S- type” fabricated from SS 304 or equivalent grade. The construction feature should be as per United States Environmental Protection Agency (EPA) regulation, Method 2, Given in Figures 1.1 and 1.2 (A)<br>ii. The construction feature shall be such that the coefficient of the pitot tube is above 0.95. |
| 3                           | Sampling probe  | Sampling probe shall be fabricated from SS 304 tube of suitable diameter (not less than 15 mm Internal diameter (ID). The SS probe should have inner glass liner to facilitate sampling for metals, acids (HCl) and PCDDs and PCDFs. Length of pitot tube and the sampling probe may correspond to user requirement.                           |

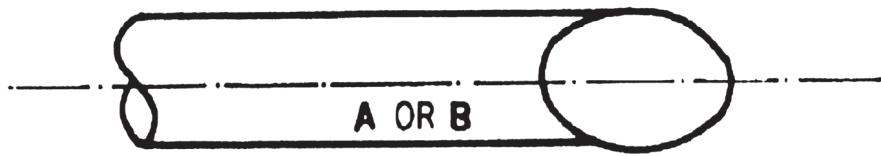
| S.N.                        | Item/Equipment                      | Specifications / Applicable ranges   |
|-----------------------------|-------------------------------------|--|
| <b>General Requirements</b> |                                     |  |
| 4                           | Nozzles                             | Nozzles shall be fabricated with SS 304 or equivalent material with internal diameters suitable to cover the full range of stack velocities. The leading edge of the nozzle should be sharp and tapered. The minimum internal diameter of the nozzle shall not be less than 4 mm. Glass nozzles are recommended for Hx and halogens, metals and PCDDs/PCDFs sampling |
| 5                           | Heated filter box                   | Heated filter box upto 200 °C with filter holder made of glass is recommended  |
| 6                           | Sample transfer line                | Heated sample transfer line (upto 200°C) made of nonreactive, non corrosive material is recommended to eliminate artifacts due to condensation   |
| 7                           | Thermocouple                        | Thermocouple sensor shall be provided with digital dial gauge capable of measuring temperature from 0 to 600 °C covered with stainless steel or mild steel casing with acid resistant treatment.   |
| 8                           | Mounting flange                     | A pair of male/female flanges fabricated with mild steel with proper hole for mounting thermocouple sensor, sampling tube and pitot tube.  |
| 9                           | Panel box sides                     | Panel box shall be fabricated with aluminium/mild steel/ fiber glass sheets with oven-baked stove–enamel finish. It should have suitable arrangement for housing stop- watch, manometer, rotameter, dry gas meter etc.   |
| 10                          | Back panel                          | Back panel shall be hinged door panel of mild steel to contain cold box with 8-10 impingers.   |
| 11                          | Inclined - cum – Vertical Manometer | Inclined- cum – vertical manometer shall be fabricated with solid acrylic sheets. It shall be provided with Inlet and outlet for filling in gauge fluid and spirit level for leveling. Velocity range of the manometer shall be 0 to 30 m/sec.   |
| 12                          | Rotameters                          | 0 to 60 lpm for particulate monitoring and 0 to 3 lpm for gaseous monitoring   |

| S.N.                        | Item/Equipment             | Specifications / Applicable ranges  |
|-----------------------------|----------------------------|---|
| <b>General Requirements</b> |                            |   |
| 13                          | Stop-watch                 | 0 to 60 minutes, one second readout with hold facility.   |
| 14                          | Impinger                   | Four number 100 ml and four to six number 225 ml capacity. Facility should be there for keeping ice at the bottom of impinge box. Electrical cooling is desirable   |
| 15                          | Connectors                 | Push and close type quick connector to ensure better leak proofness   |
| 16                          | Vacuum pump                | Vacuum pump shall be of rotary design, with a capacity of 0 to 120 lpm gas flow with single phase motor, 220 V. The pump shall also have a moisture trap and air inlet valve. It shall be mounted inside pump housing and shall be portable         |
| 17                          | Dry gas meter              | The sampling train shall have a dry gas meter. The capacity of the meter should be adequate to record upto 60 lpm of airflow and a minimum readout of 0.001 cubic meters.   |
| 18                          | Pump housing               | Mild steel case with oven-baked stove enamel finish and ON/OFF switch with indicator lights.  |
| 19                          | Tools                      | A Kit containing the essential tools for connecting various components shall be provided with the equipment.  |
| 20                          | Isokineticity              | The kit shall be capable to perform continuous monitoring of isokinetic condition throughout the sampling period  |
| 21                          | Temperature metering point | at Temperature measuring device at metering point shall be provided (0-50 °C)   |
| 22                          | Vacuum measurement         | Digital/analog vacuum pressure drop measurement device in mm Hg should be provided in stack kit.  |
| 23                          | Train leakages             | The sampling train shall be tested for leakage by plugging the inlet. The rotameter shall not give a reading beyond 5 lpm when the flow has been set at 100 lpm. The dry gas meter shall also give a reading of less than 5 percent of the airflow. |





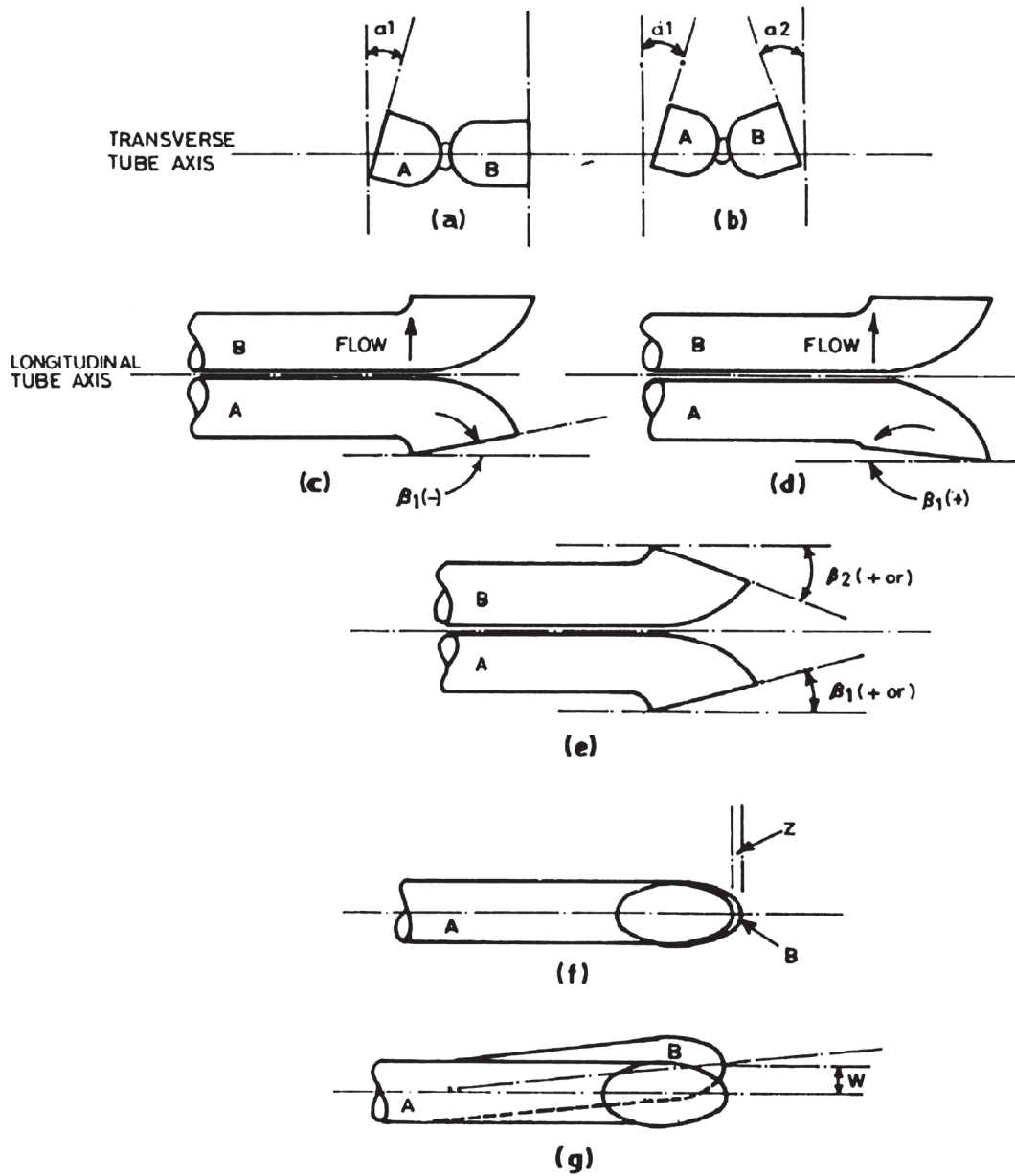
(a)



(b)

Properly constructed Type S pitot tube shown in: a) Top view; face opening planes parallel to longitudinal axis; b) side view; both legs of equal length and central lines coincident, when viewed from both sides. Baseline coefficient values of 0.84 may be assigned to pitot tubes constructed this way.

**FIGURE 1.1 "S - TYPE" pitot tube construction**



Types of face opening misalignment that can result from field use or improper construction of type S pitot tubes. These will not effect the baseline of  $C_p(s)$  so long as  $\alpha_1$  and  $\alpha_2 < 10^\circ$ ,  $\beta_1$  and  $\beta_2 < 5^\circ$ .  $z < 0.32$  cm (1/8 in.) and  $w < 0.08$  cm (1/32 in.)

FIGURE 1.2 (A) 'S - TYPE' pitot tube construction

## 1.2 Method of Testing

### 1.2.1 Molecular weight determination

Dry and wet molecular weights

Equation 1 is used to calculate the dry molecular weight of flue gas. This equation may be modified with terms if other gaseous constituents that will influence the molecular weight if present. Equation 2 is used to calculate the molecular weight of the sample is used to calculate the molecular weight of the gas on a wet basis.

Calibrated multiple combustion gas analyzer may be used to know the percentile composition of flue. Orset analysis may also serve the same purpose.

$$M_d = 0.44 (\%CO_2) + 0.32 (\% O_2) + 0.28(\% N_2 + \% CO) + \dots \quad \text{Eq - 1}$$

$$M_s = M_d (1 - B_{wO}) + 18 B_{wO} \dots \quad \text{Eq - 2}$$

Where,

0.44 – molecular weight of carbon dioxide divided by 100, kg/kg-mole

0.32 – molecular weight of oxygen divided by 100, kg/kg –mole

0.28 – molecular weight of nitrogen and carbon monoxide divided by 100, kg kg-mole

$B_{wO}$  – proportion by volume of water vapour in stack gas.

18 - molecular weight of water, Kg / Kg -mole

*Note: %  $N_2$  is calculated by difference. In the majority of cases the following equation may be used:*

$$\% N_2 = 100 - (\% CO_2 \text{ avg} + \% O_2 \text{ avg} + \% CO \text{ avg.})$$

Where,

$M_d$  = molecular weight of stack gas on dry basis, kg / kg –mole.

$M_s$  = molecular weight of stack gas on wet basis, kg / kg –mole

$\% CO_2$  = Percent CO2 by volume, dry basis

$\% O_2$  = Percent oxygen by volume, dry basis

$\% N_2$  = percent nitrogen by volume, dry basis

### 1.2.2 Static pressure determination

For the static pressure determination requires first to disconnect the positive end of the pitot tube then take the reading of velocity pressure. Use the following formula for the calculation. For measurement of static gas pressure pitot tube should be rotated by 90° from the position of actual  $\Delta P$  measurement. This would provide better accuracy.

$P_s$  may be calculated as

$$P_s = P_{\text{bar}} \pm (\Delta P_s / 13.6)$$

Where:

$P_{\text{bar}}$  = Barometric pressure in mm mercury column

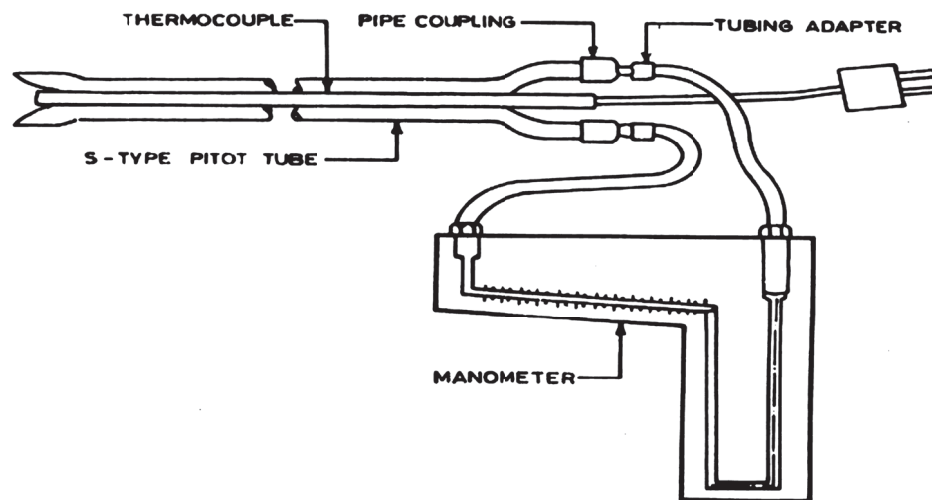
$\Delta P_s$  = Stack gas velocity pressure, mm water column

$P_s$  = Static pressure mm Hg column.

Density of Hg = 13.6

### 1.2.3 Stack gas velocity determination

For velocity determination connect pitot tube to the stack as given in Fig 1.2 (B). The dynamic and a static pressure are measured by using the manometer. The temperature inside the duct is also measured. The velocity of gas in the duct and the air quantity are determined using the following formula.



**FIGURE 1.2 (B) “S – TYPE” pitot tube and inclined manometer assembly**



### 1.2.3.1 Preliminary determination

Preliminary determination requires for the parameters like Temperature (Stack & ambient temperature °C), velocity pressure Head  $\Delta P$ , Barometric pressure, Static pressure as mentioned in the above paragraph.

$$U_s = K_p \times C_p \times (\Delta P)^{1/2} \left[ T_s / (P_s \times M_s) \right]^{1/2}$$

Where

$U_s$  = Stack gas velocity, m/s

$K_p$  = Constant, 33.5

$C_p$  = S- type pitot tube coefficient.

$T_s$  = absolute stack gas temperature, °K

$P$  = Stack gas velocity pressure, mm water column

$P_s$  = Absolute stack gas pressure, mm Hg

$M_s$  = Molecular weight of stack gas on wet basis, Kg / Kg –mole

### 1.2.3.2 Stack gas volumetric flow Rate

The following equation is used to calculate the stack gas volumetric flow rate,  $Q_s$  ( $m^3$  hr).

$$Q_s = 3600 (U_s) \times A_s (1 - B_{wO}) \times (T_{ref} / T_s) \times (P_s / P_{ref})$$

$A_s$  = Area of the stack (duct),  $m^2$

$B_{wO}$  = Proportion by volume of water vapour in stack gas.

$T_{ref}$  = 298 °K

$P_{ref}$  = 760 mm of Hg

$T_s$  = Absolute stack gas temperature, °K

$P_s$  = Absolute stack gas pressure

### 1.2.4 Moisture determination

The moisture content may be determined either by condenser method or by wet / dry bulb method temperature and then referring to a suitable psychrometric chart. Latter should be limited to non-acid gas streams with moisture content of less than 15 percent and dew point less than 52° C. The condenser method works well for most gas streams and also relative easy to perform.

### 1.2.4.1 Condenser method

The condenser method, in principle, involves extracting a sample of the stack gases through a filter for removal of the particulate matter, then through a condenser, accumulating the condensate formed in process. The object of the test is to collect and measure the volume of all the condensate formed at the condensing temperature from a measured amount of gas.

Apparatus – The apparatus necessary for determination of moisture content by the condensate method is given below.

| S.No | Apparatus                      | Description  |
|------|--------------------------------|--|
| 1    | Particulate Sampling Apparatus | Consisting of a probe of stainless steel or pyrex glass sufficiently heated to prevent condensation and equipped with a filter to remove particulate matter.   |
| 2    | Condenser                      | It is equipped with temperature gauge. This may be substituted with two condenser bottles in an ice bucket each with 30 ml capacity or equivalent. The condenser /condenser bottles are filled with chilled water. |
| 3    | Dry Gas Meter                  | To measure within 5 percent of the total sample volume   |
| 4    | Gauges                         | Two thermometers (range 0 – 100 °C), two calibrated vacuum gauges or U- tube manometers (range 0 – 500 mm mercury).  |
| 5    | Gas Pump                       | Leak free diaphragm type or equivalent, for sucking gas through sampling apparatus   |
| 6    | Fittings                       | Tubing (rubber, neoprene, etc.), rubber stoppers and flow control (needle- valve and shut –off ball valve).  |

Procedure – Except in unusual circumstances, the water vapour is uniformly dispersed in the gas stream and therefore sampling for moisture determination need not be isokinetic and is not sensitive to position in the duct. The sampling nozzles may be positioned down –stream to minimize the build up of pressure drop across the thimble due to particulates catch. Sample the gas at a rate of about 500 ml/ sec. Run the test until enough condensate has been collected to enable an accurate measurement. Measure the temperature and pressure

of condenser close to the meter, as an insignificant pressure loss in the line between them is expected. The meter pressure may be substituted for condensate pressure also in order to calculate the moisture content. Measure the volume of condensate collected in a graduated measuring cylinder.

### Calculations

**Calculate the volume of water vapour collected using the following equation:**

$$V_v = \frac{(V_c \times 22.4)}{1000 \times 18} \times \frac{T_m}{273} \times \frac{760}{P_{\text{bar}} - P_m}$$

$V_v$  = Equivalent vapour of condensate under sampling condition,  $\text{m}^3$

$V_c$  = Volume of condensate in condensor, ml

$T_m$  = Temperature at metering condition,  $^{\circ}\text{K}$

$P_m$  = Suction at meter, mm mercury column

$P_{\text{bar}}$  = Barometer pressure, mm mercury column

**Calculate the moisture content of the gases using the following equation:**

$$B_{\text{wo}} = \frac{V_v}{V_v + V_m}$$

$$M = \frac{V_v}{V_v + V_m} \times 100$$

Where

$M$  = Moisture in the flue gases, percent

$V_v$  = Equivalent vapour volume of condensate under sampling condition.

$V_m$  = Volume of gas sampled ( $\text{m}^3$ )

#### 1.2.4.2 Wet / dry bulb method

The equilibrium temperature attained by water, which is vapourizing adiabatically into gas of composition and constant dry bulb or actual temperature, is termed as wet bulb temperature. The amount of depression of the wet bulb temperature below the dry

bulb temperature is a function of the degree of saturation of the humidity of the gas. Therefore, the moisture content of the gas can be determined from the wet and dry bulb temperature.

Calculations – the moisture content may be determined from the test data using a psychrometric chart. The percentage water vapour by volume is found directly. Inputs are the dry bulb temperature and wet bulb temperature.

### 1.3 Selection of Sampling Site and Minimum Number of Traverse Points

Select the sampling site at any cross section of the stack or duct that is at least eight stack or duct diameters downstream and two diameters upstream from any flow disturbance such as bend, expansion, contraction, visible flame, or stack exit (see inlet, Figure 1.3). For rectangular cross section, the larger dimension shall be used to represent the stack diameter.

1.3.1 When the above sampling site criteria can be met, determine the minimum number of traverse points required, from Table 1.3. The minimum required number of traverse points is a direct function of stack or duct diameter.

1.3.2 When a sampling site such as described in 1.3 is not accessible, choose a convenient sampling location and use Table 1.3 and Figure 1.3 to determine the minimum required number of traverse location to the nearest upstream and downstream disturbance. First, measure the distance from the chosen sampling location to the nearest upstream and downstream disturbance.

1.3.3 Then, from Figure 1.3 determine the corresponding sample points multiples for both distances and select the greater of these. Multiply it by the number obtained from Table 1.3. The result of this calculation is the minimum number of traverse points required. This number may have to be increased such that for circular stacks the number is a multiple of 4 and for rectangular stack the number follows the criteria given in 1.3.4.

1.3.3 Cross- section layout and location of traverse points For circular stack divide the cross section into equal parts by two right- angle diameters. Locate half the traverse points symmetrically along each diameter according to Figure 1.4 and Table 1.4.

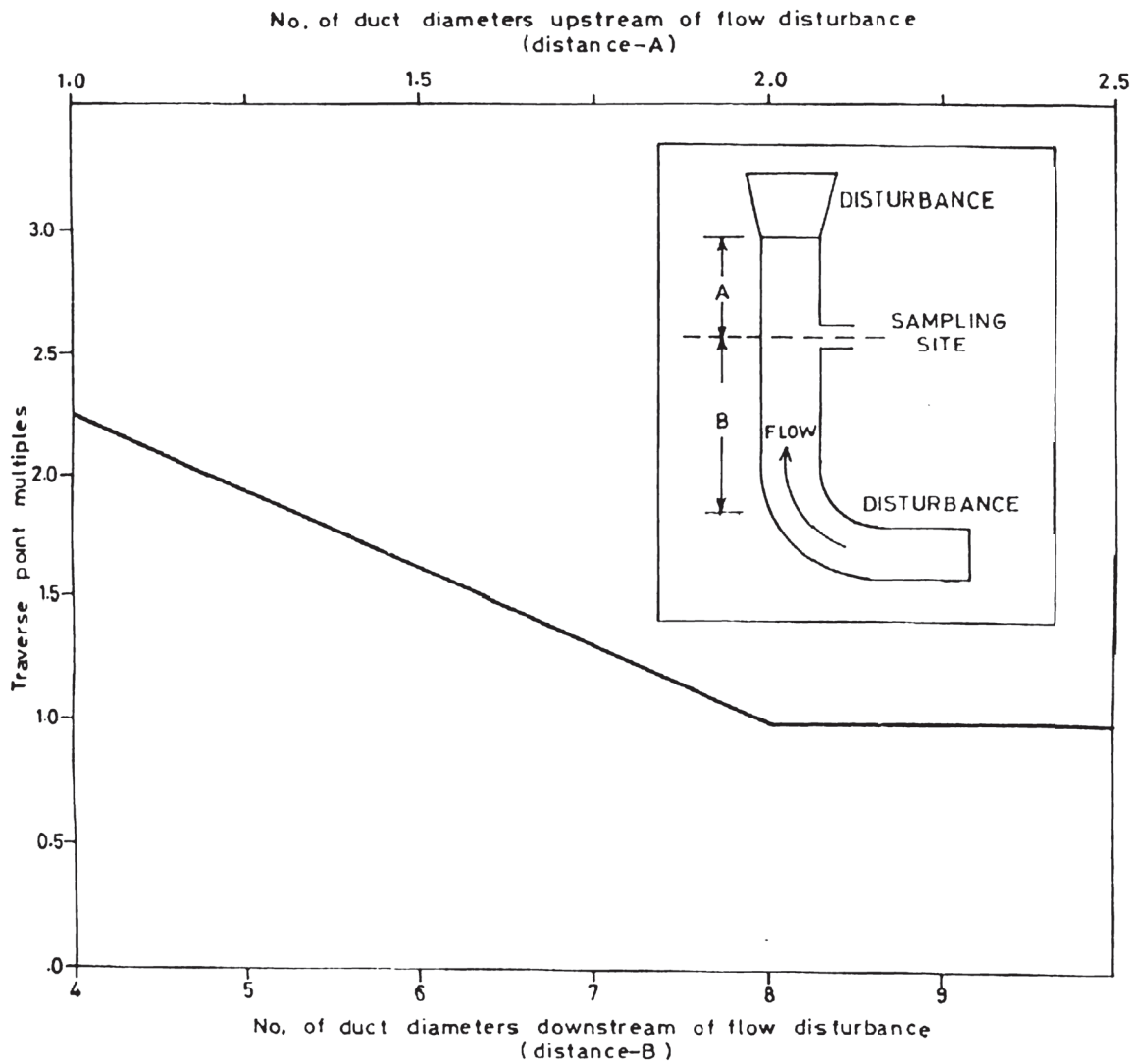
1.3.4 For rectangular areas as there are traverse points as many equal rectangular areas traverse points such that the ratio of the elements/ area is between one and two. Locate the traverse points at the centroid of each area according to Figure 1.4.

1.3.5 Under no condition shall sampling points be selected within 3 cm of the stack wall.

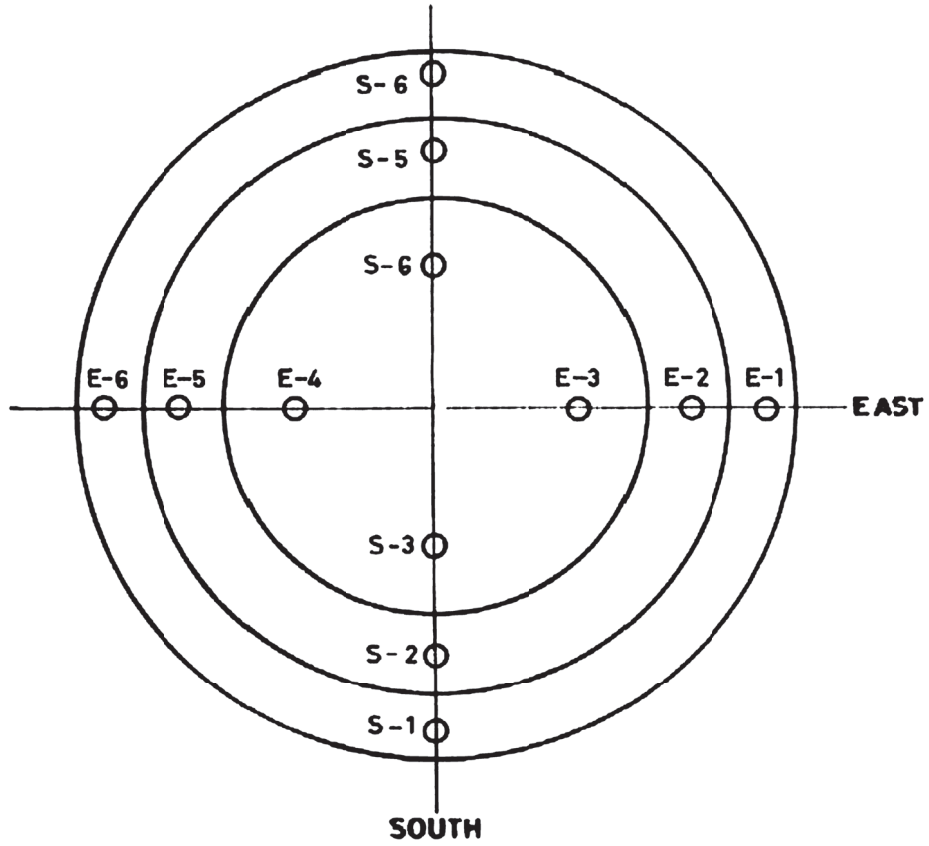


**Table 1.3 : Minimum required number of traverse points for sampling sites which meet specified criteria**

| Inside diameter of stock of duct (m) | Number of points |
|--------------------------------------|------------------|
| $I.D. \leq 0.3$                      | 4                |
| $0.3 \leq I.D. \leq 0.6$             | 8                |
| $0.6 \leq I.D. \leq 1.2$             | 12               |
| $1.2 \leq I.D. \leq 2.4$             | 20               |
| $2.4 \leq I.D. \leq 5$               | 32               |



**FIGURE 1.3 Travers point multiples to determine minimum number of traverse points requirement when a <2 dia or b <8 dia**



|          |          |          |          |          |
|----------|----------|----------|----------|----------|
| <b>A</b> | A-1<br>○ | A-2<br>○ | A-3<br>○ | A-4<br>○ |
| <b>B</b> | B-1<br>○ | B-2<br>○ | B-3<br>○ | B-4<br>○ |
| <b>C</b> | C-1<br>○ | C-2<br>○ | C-3<br>○ | C-4<br>○ |

FIGURE 1.4 Location of traverse points on circular and rectangular cross section divided into twelve equal areas

**TABLE-1.4 Location of traverse points on diameters of cross section of circular stacks**

| TRAVERSE POINT NUMBER ON A DIAMETER | PERCENT OF STACK DIAMETER FROM INSIDE WALL TO TRAVERSE POINT |      |      |      |      |      |      |      |      |      |      |      |
|-------------------------------------|--|------|------|------|------|------|------|------|------|------|------|------|
|                                     | Number of traverse points on a diameter                      |      |      |      |      |      |      |      |      |      |      |      |
|                                     | 2  | 4    | 6    | 8    | 10   | 12   | 14   | 16   | 18   | 20   | 22   | 24   |
| 1                                   | 14.6   | 6.7  | 4.4  | 3.3  | 2.5  | 2.1  | 1.8  | 1.6  | 1.4  | 1.3  | 1.1  | 1.1  |
| 2                                   | 85.4   | 25.0 | 14.7 | 10.5 | 8.2  | 6.7  | 5.7  | 4.9  | 4.4  | 3.9  | 3.5  | 3.2  |
| 3                                   |  | 75.0 | 29.5 | 19.4 | 14.6 | 11.8 | 9.9  | 8.5  | 7.5  | 6.7  | 6.0  | 5.5  |
| 4                                   |  | 93.3 | 70.5 | 32.3 | 22.6 | 17.7 | 14.6 | 12.5 | 10.9 | 9.7  | 8.7  | 7.9  |
| 5                                   |  |      | 85.3 | 67.7 | 34.2 | 25.0 | 20.1 | 16.9 | 14.6 | 12.9 | 11.6 | 10.5 |
| 6                                   |  |      | 95.6 | 80.6 | 65.8 | 35.5 | 26.9 | 22.0 | 18.8 | 16.5 | 14.6 | 13.2 |
| 7                                   |  |      |      | 89.5 | 77.4 | 64.5 | 36.6 | 28.3 | 23.6 | 20.4 | 18.0 | 16.1 |
| 8                                   |  |      |      | 96.7 | 85.4 | 75.0 | 63.4 | 37.5 | 29.6 | 25.0 | 21.8 | 19.4 |
| 9                                   |  |      |      |      | 91.8 | 82.3 | 73.1 | 62.5 | 38.2 | 30.6 | 26.1 | 23.0 |
| 10                                  |  |      |      |      | 97.5 | 88.2 | 79.9 | 71.7 | 61.8 | 38.8 | 31.5 | 27.2 |
| 11                                  |  |      |      |      |      | 93.3 | 85.4 | 78.0 | 70.4 | 61.2 | 39.3 | 32.3 |
| 12                                  |  |      |      |      |      | 97.9 | 90.1 | 83.1 | 76.4 | 69.4 | 60.7 | 39.8 |
| 13                                  |  |      |      |      |      |      | 94.3 | 87.5 | 81.2 | 75.0 | 68.5 | 60.2 |
| 14                                  |  |      |      |      |      |      | 98.2 | 91.5 | 85.4 | 79.6 | 73.9 | 67.7 |
| 15                                  |  |      |      |      |      |      |      | 95.1 | 89.1 | 83.5 | 78.2 | 72.8 |
| 16                                  |  |      |      |      |      |      |      | 98.4 | 92.5 | 87.1 | 82.0 | 77.0 |
| 17                                  |  |      |      |      |      |      |      |      | 95.6 | 90.3 | 85.4 | 80.6 |
| 18                                  |  |      |      |      |      |      |      |      | 98.6 | 93.3 | 88.4 | 83.9 |
| 19                                  |  |      |      |      |      |      |      |      |      | 96.1 | 91.3 | 86.8 |
| 20                                  |  |      |      |      |      |      |      |      |      | 98.7 | 94.0 | 89.5 |
| 21                                  |  |      |      |      |      |      |      |      |      |      | 96.5 | 92.1 |
| 22                                  |  |      |      |      |      |      |      |      |      |      | 98.9 | 94.5 |
| 23                                  |  |      |      |      |      |      |      |      |      |      |      | 96.8 |
| 24                                  |  |      |      |      |      |      |      |      |      |      |      | 98.9 |

#### 1.4 Location of Sampling Port

To ensure laminar flow, sampling ports shall be located at least 8 times chimney diameter downstream and 2 times upstream from any flow disturbance. For a rectangular cross section the equivalent diameter (De) shall be calculated by using following equation to determine up stream, downstream distances.

$$De = (2 L X W) / (L+W)$$

Where, L = Length in m, W= width in m.

Sometimes it may so happen for existing chimneys that sufficient physical chimney height is not available for desired sampling locations. In such cases additional traverse points shall be taken as explained at section 1.3.

#### **1.4.1 Number of sampling ports**

The pitot tubes commercially available in the country generally do not exceed 2 meter in length. Any points on the horizontal cross- section of a stack (chimney) along any diameter can be measured for flow by the pitot tube, if the point is approachable. Inserted pitot tube through the sampling port (hole) for stacks with diameter less than 2m. Minimum two (mutually orthogonal) sampling ports are required in a circular chimney, so that full stack cross-sectional area can be covered for measurements. For stacks having diameter between 2 and 4 meters, two mutually orthogonal sampling ports are to be increased to four by providing additional sampling ports at diametrically opposite position, to the first two sampling ports (Fig 1.5)

#### **1.4.2 Dimensions of sampling port**

Port Type: Pitot tube, temperature and sampling probe are to be inserted together into the sampling port for monitoring purposes. Sampling port should be a standard flanged pipe of 0.10 m inside diameter (ID) with 0.15 m bolt circle diameter. An easily removable blind flange should be provided to close the port when not in use. Port Installation: Flanged pipe used as port should be installed with the interior stack wall. Port should extend outward from the exterior stack wall not less than 50 mm and not more than 200 mm only when additional length is required for gate valve installation. Ports should be installed at a height between 0.90 and 1.2 m above the floor of the working platform. Port Loading: The port installation should be capable of supporting the following loads:

Vertical shear of 91 Kg

Horizontal Shear of 23 Kg and

Radial tension of 23 Kg (along stack diameter)

#### **1.4.3 Features of platform for stack sampling**

Size and extent of platform for sampling: If two ports are required at 90 degree the work platform should serve that half of the stack circumference between the ports and extend at least 1.2 meters beyond each port. If four ports are required at 90 degree, the work platform should serve the entire circumference of the stack. Minimum platform width shall always be 1.2 meters regardless of diameter of stack and number of sampling ports. A typical platform for sampling is shown in Figure1.6.

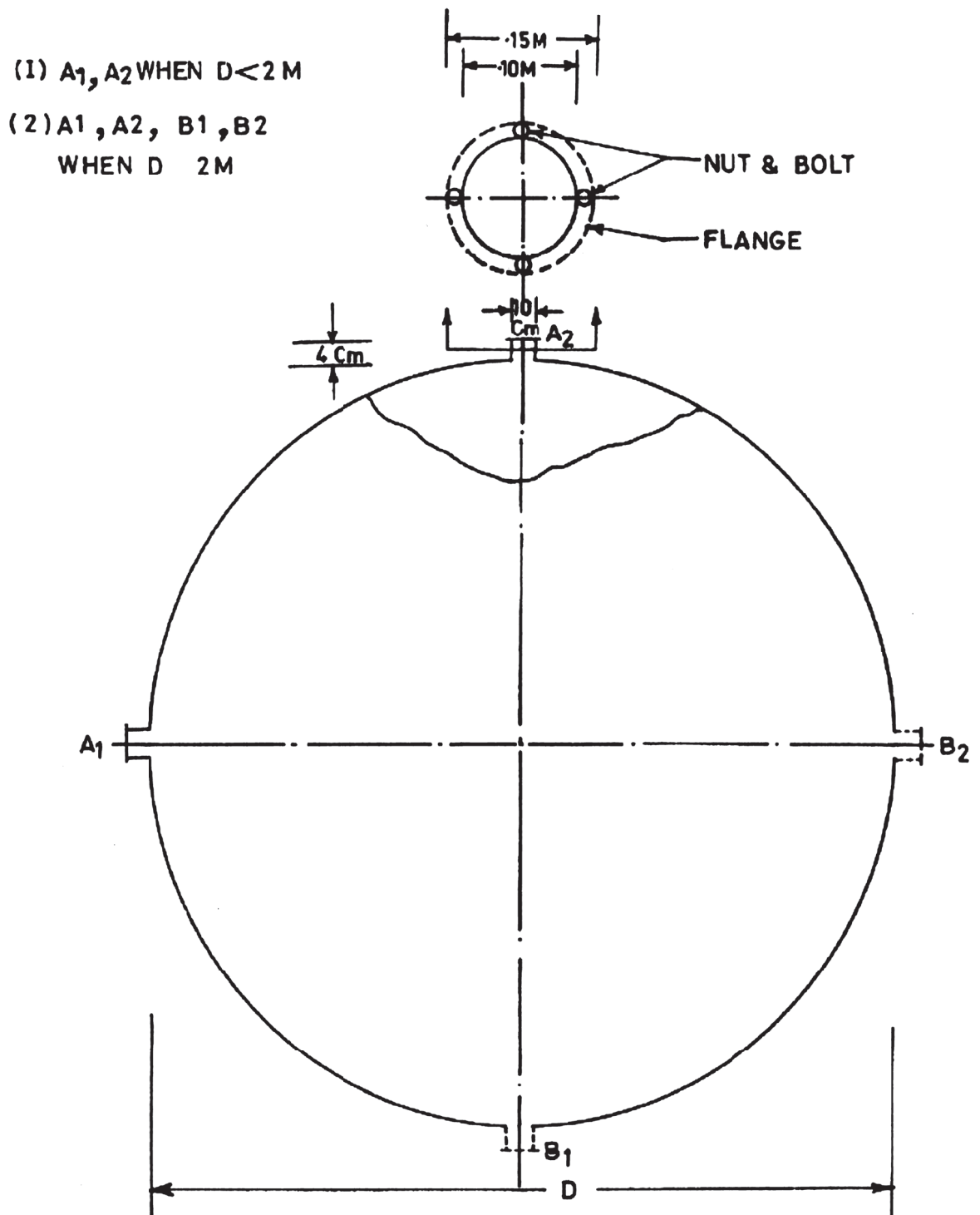


FIGURE 1.5 Position of sampling ports in a circular chimney

#### **1.4.4 Platform access**

Safe and easy access to the work platform should be provided via caged ladder, stairway, or other suitable means.

Guardrails, Ladder wells and Stairwells: A safe guardrail should be provided on the platform. Angular rail is preferable than round rail member. No ladder well, stairwell, or other such openings should be located within 1 meter of any port. Ladderwells should be covered at the platform. Any stairwell leading directly to the platform should be equipped with a safety bar at the opening.

#### **1.4.5 Platform loading**

The work platform should be able to support at least three men (Average 80 Kg each) and 91 Kg of test equipment (stack monitoring kit, etc.). If the stack exists through a building roof, the roof may suffice as the work platform, provided the minimum test sites required are complied with.

#### **1.4.6 Clearance zone**

A three- dimensional, obstruction free clearance zone should be provided around each port. The zone should extend 0.6 m above, below, to either side of the port. The zone should extend outward from the exterior wall of the stack to a distance of at least 3 meters. The clearance zone is illustrated in Figure 1.6.

#### **1.4.7 Power Supply**

Power supply shall be as follows:

- A. Platform- one 220 volts, 15 amp, single phase AC circuit with a grounded, two receptacle weatherproof outlets.
- B. Stack base- one 220 volts, 15 amp, single phase AC circuit with a grounded, two receptacle weatherproof outlet.

#### **1.4.8 Vehicle access and parking**

Except for situations in which sampling operation must be conducted from a rooftop or similar structure, stack sampling is sometimes coordinated and controlled from a monitoring van, which is usually parked near the base of the stack for the duration of the sampling period. Vehicle access and parking space must be provided, since various equipment transport lines will be strung from the monitoring van to the stack platform and will remain in position during the sampling.

#### **1.4.9 Additional requirements**

In addition to above aspects, the sampling platform, guardrails etc. should also be regularly painted and checked for corrosion. There should be no leakage around the sampling

port (specially needed for stacks emitting corrosive chemicals). If anticorrosive lining is done inside the chimney, the same should be extended to the projected portion of the sampling port, monolithically. Improper lining at the port reduces chimney life considerably. Sampling port should be air tight and moist air should not be allowed to enter the chimney

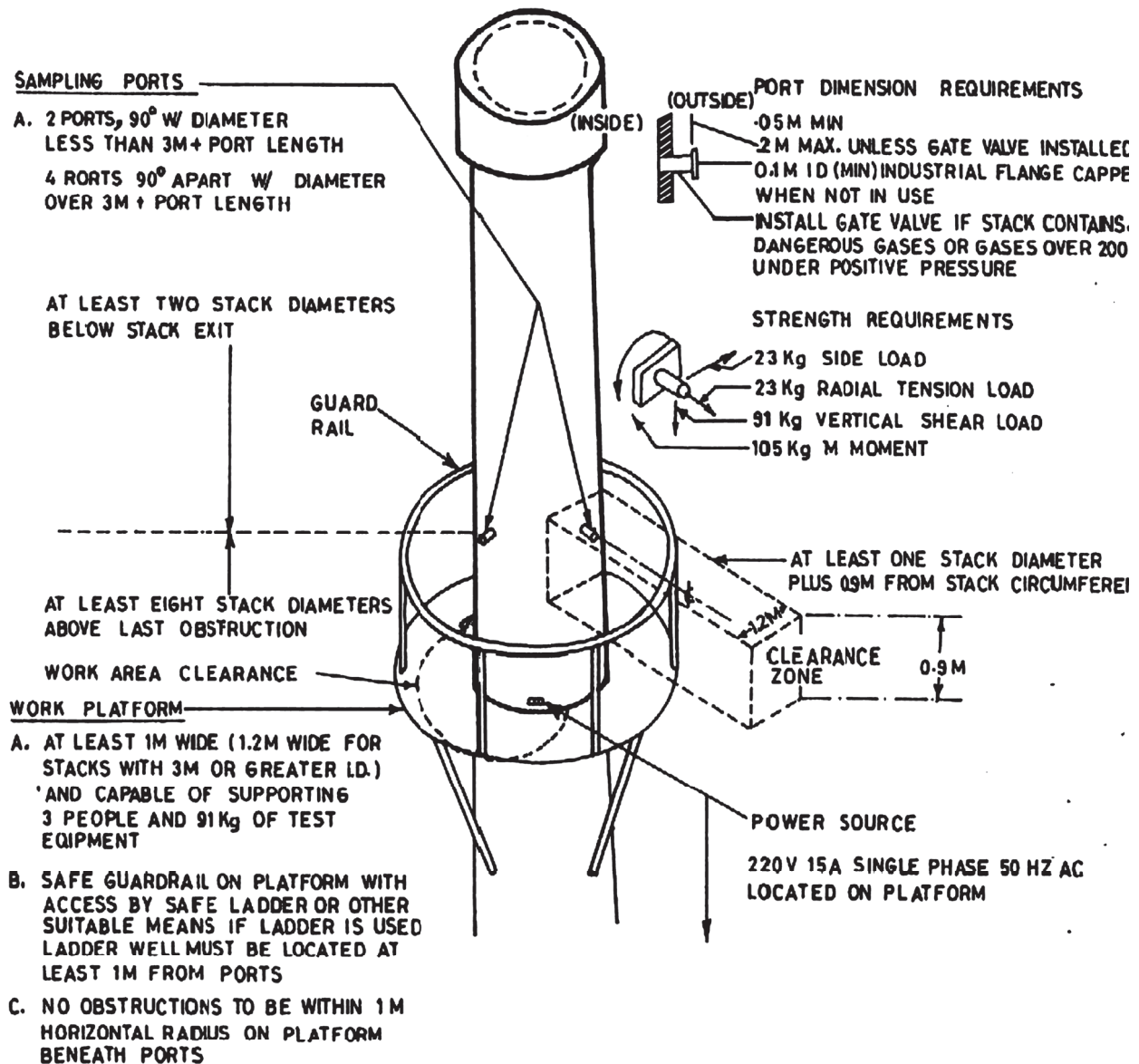


FIGURE 1.6 Typical sampling provision

## 2.0 REFERENCES

1. Comprehensive Industry Document Series: COINDS/ 20/ 1984 - 85, Central Pollution Control Board



**Method – 1**  
**(Part- II)**  
**Determination of particulate matter emissions from stationary sources**

## **1.0 PRINCIPLE**

Determination of particulate concentration consists of isokinetic sampling of a measured amount of gas from the flue gases and separating the particles from the gas and hence determining the particulate concentration. To ensure representative sample, the kinetic energy of the gas stream in the stack should be equal to kinetic energy of the gas stream through the sampling nozzle.

## **2.0 APPLICABILITY**

This method is applicable for determination of particulate matter (PM) emissions from stationary sources. This is for sampling of particulate matter in a moving gas stream in a duct or a stack. These procedures utilize particulate filtering systems, which are located within the stack. If properly used, these systems are satisfactory for determining the mass concentration of particulate matter in the gas stream at stack condition. The use of collection systems located outside the stack for collecting samples at other than in-stack condition is an alternative.

## **3.0 INTERFERENCES**

It has been observed that, if sampling velocity is greater than the isokinetic rate, the sampling will have a lower mass concentration of particulate material than the main stream because of greater percentage of fine particles. However, if the sampling velocity is less than the isokinetic rate, the particulate sample has a higher mass concentration than actually present, with lower concentration of fine particles.

## **4.0 SAMPLING**

Sampling at other than isokinetic velocities induces errors for two reasons. First, sampling at greater or less than isokinetic rates tend to cause respectively a larger or a smaller volume to be withdrawn from the flue gases than accounted for by the cross section area of the probe. Secondly, particles greater than 3.5 micron in size have sufficient inertia so that particle motion may deviate significantly from the gas flow streamline pattern.

### **4.1 The Sampling Consists of Several Distinct Steps. Refer 1.2 of Stack monitoring – Material and Methodology for Isokinetic Sampling (Method1)**

## **5.0 PROCEDURE FOR PARTICULATE MATTER DETERMINATION**

### **5.1 Selection of Location of Sampling**

Sample for particulate concentration shall be done at the same traverse points where velocity measurements were carried out.

## 5.2 Calculation of Proper Sampling rate

The meter for measuring the gas sample measures the gas at conditions of temperature, pressure and moisture content which are different than those in the flue. Therefore, calculate the sampling rate at the gas meter for each sampling points before starting the test and record on the log the required rate (Table-2).

**Calculate the sampling rate at the gas meter as follows:**

$$V_v = R_s \times \frac{T_m}{T_s} \times \frac{P_{\text{bar}} - P_s}{P_{\text{bar}} - P_m} \times \frac{V_m}{V_m + V_v}$$

Where

$R_m$  = flow rate through meter,  $\text{m}^3/\text{s}$

$R_s$  = Sampling rate at nozzle, LPM

$T_m$  = Absolute temperature in metering conditions,  $^{\circ}\text{K}$

$T_s$  = Absolute stack gas temperature,  $^{\circ}\text{K}$

$P_s$  = Absolute stack gas pressure, mm mercury column

$P_{\text{bar}}$  = Barometer pressure, mm mercury column

$P_m$  =  $(P_{m1} - P_{m0}) / 2$  Suction at meter, mm mercury column

$V_m$  = Volume of gas sampled at meter conditions,  $\text{m}^3$

$V_v$  = equivalent vapour volume of condensate at meter conditions,  $\text{m}^3$

*Note: Take initial reading of vacuum gauge ( $P_{m0}$ ) in mm Hg at the starting of sampling and final vacuum pressure ( $P_{m1}$ ) in mm Hg just before putting off the pump, when sampling is complete. Calculate average difference in suction pressure, referred as  $P_m$*

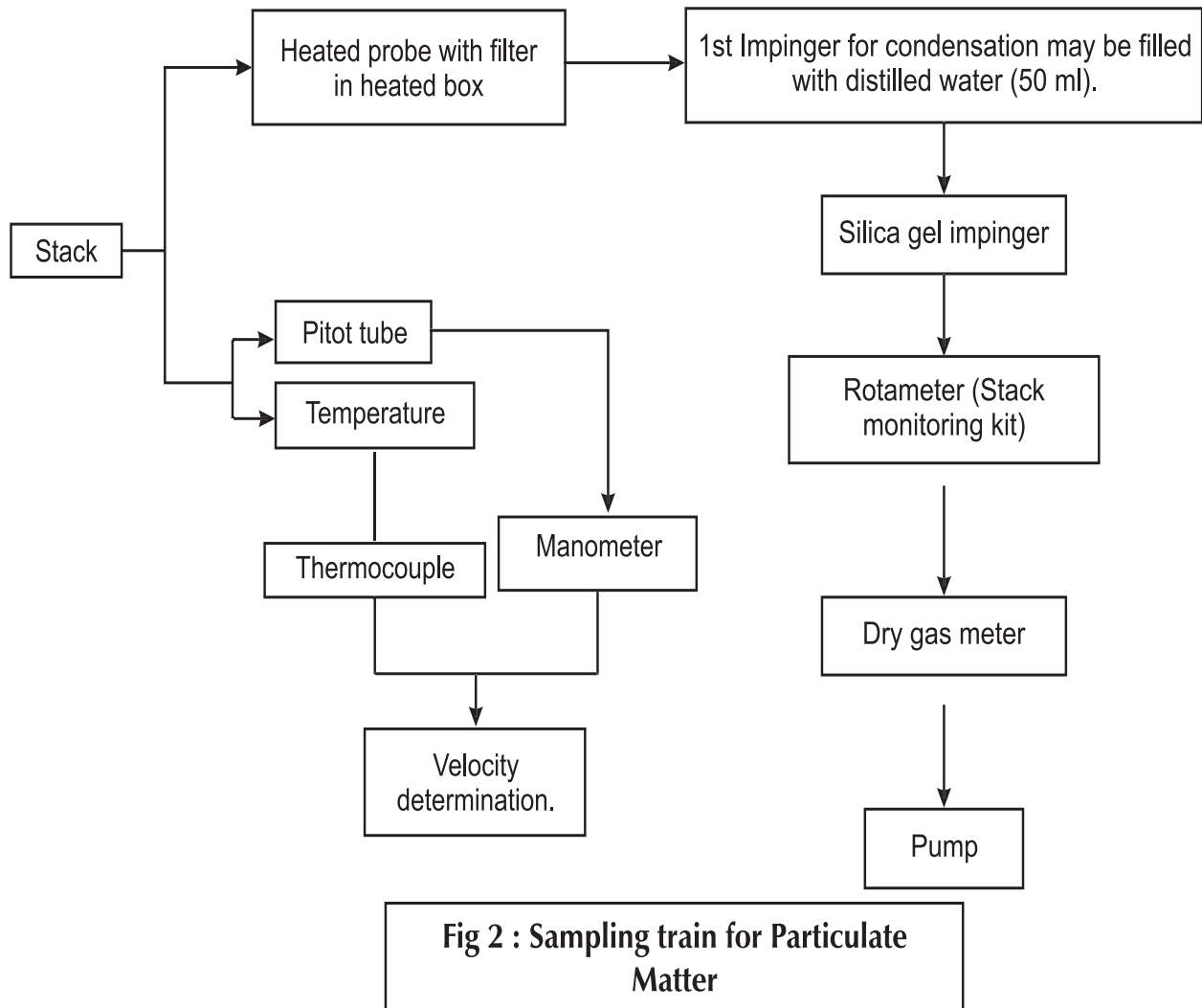
5.3 Select the nozzle size, which provide a meter-sampling rate between 40 to 60 lit / min. Charts relating sampling rate with stack and meter condition may be prepared for the range of condition expected. Duration of Sampling- Deem the run to be of sufficient length if one of the following criteria has been obtained:

- a. A minimum of  $1 \text{ m}^3$  of dry gas has been withdrawn for sampling.
- b. The mass of particulate matter amounts to atleast 20 percent of the mass of the filtering medium in the sampler.

Experience and intelligent judgment should be applied in determining the sampling time. Too short a time, may give unreliable result and too long a time may cause the resistance of the sampling train to exceed the pump's limits.

#### 5.4 Preparation of the Sampling Train

- After proper nozzle and filtering medium have been selected assemble the sampling train as shown in **Figure 2**
- Mark the sampling probe (including nozzle and filter holder) with the same traverse points used for conducting the velocity traverse.
- Place a clean, pre-weighted thimble/filter in the filter holder and tighten securely.
- Start the test after sampling rates have been calculated and train assembled & checked for leakages. When the equipment is ready in all respects, record the initial dry gas meter reading and push the sampling probe carefully into the duct to the point nearest to the back wall. This will allow the probe to cool in hot stack as it comes out, shortening the time required for cooling after the sample is taken. It is advisable to allow the nozzle and filter holder to preheat so that moisture present in the gases does not condense in the filter initial part of the sampling.
- When starting the test, the nozzle should be facing in the upstream direction, start operating the suction source, open the control valve and start the stop watch. Note the time and record it in the log sheet. Adjust the flow rate with the help of rotameter and control valve until the desired flow rate for isokinetic condition is obtained. As the test proceeds, dust collected in the thimble/ filter increases the amount of suction required to maintain proper meter rate. Valve should be adjusted accordingly. This suction should not exceed 150 mm of mercury for paper thimble / filter. In case it exceeds this value before the completion of sampling, replace the same with a new thimble and restart sampling. During the test, if the mercury suction pressure at the meter drops suddenly it indicates that a leak has developed in the equipment or that thimble/filter has cracked. Record the initial gas meter reading and pressure and temperature in the sampling train as well as condensor temperature at half – minute's interval during the test.
- When sampling at one point has been completed, move the sampling probe to the next point as quickly as possible. At the completion of test, close the control valve, turn the direction of the probe so that the sampling nozzle is facing down- stream and record the final gas volume and time. Remove the sampler carefully from the flue and plug the nozzle to prevent the loss of sample.



## 6.0 SAMPLE RECOVERY

After the sampler has cooled, brush down the dust on the inside of the nozzle carefully into the thimble using a small brush. Then, remove the thimble and place it in a dust tight container for transportation to the weighing room. In case the filter holder is kept outside during the sampling, the dust from the sampling probe before the filter holder should be brushed down into the filter.

Determine the mass of dust collected in the thimble by difference in weighing, that is, by weighing the thimble before and after the run. Dry the thimble in an oven for about 2 hours at 120 °C prior to sampling. After sampling, cool it and dry again for weighing the thimble along with dust maintaining the same condition as prior to sampling.

## 7.0 CALCULATIONS

Calculate the volume of gas sampled using the following equation: Volume of dry gas through the sampling train (25 °C 760 mm Hg )

$$V_{std} = V_m Y \frac{P_{bar} - P_m}{760 \text{ mm Hg}} \times \frac{273 + 25 \text{ }^\circ\text{C}}{T_m + 273}$$

Where

$T_m$  = Temperature of gas at dry meter condition,  $^\circ\text{C}$

$V_m$  = Volume of gas sampled at dry gas meter conditions,  $\text{m}^3$

$(P_{bar}-P_m)$  = Actual pressure in sampling train, mm mercury column.

$P_m$  = Suction at meter, mm mercury column

$P_{bar}$  = Barometric pressure in sampling train, mm mercury column.

$Y$  = Calibration factor of dry gas meter.

### 7.1 Dust Concentration

Calculate the dust concentration using the following equation:

$$E_M = \frac{(W_2 - W_1)_m \text{ gm} \times 1000}{V_{std}}$$

Dust Concentration in  $\text{mg} / \text{Nm}^3$ ,

( $25^\circ\text{C}$ , 760 mm Hg, dry basis)

Where

$V_{std}$  = Volume of dry gas through the meter

( $25^\circ\text{C}$ , 760 mm Hg),  $\text{Nm}^3$

$W_1$  = Initial weight of filter paper

$W_2$  = Final weight of filter paper

$\text{O}_2$  correction is only carried out, if  $\text{O}_2$  corrections  $> 11\%$ . For  $\text{O}_2 < 11\%$ . No correction is allowed.

It's require to correct the value for the 11%  $\text{O}_2$  by following formula

$$E_s = \frac{21 - O_s}{21 - O_m} \times E_M$$

Similarly in case of  $\text{CO}_2$  (12%) correction

$$E_s = E_m \frac{12}{\% \text{CO}_2 \text{ observed}}$$

No correction for  $\text{CO}_2 > 12\%$

$E_s$  = calculated emission concentration at the standard percentage oxygen concentration

$E_M$  = measured emission concentration

$O_s$  = standard oxygen concentration

$O_M$  = measured oxygen concentration

### 7.3 Emission Rate

Calculate the dust emission rate as follows:

$$\text{Dust Emission Rate} = \frac{E_M \times Q_S}{10^6}$$

Where

$Q_S$  = flue gas flow rate ( 25 °C, 760 Hg mm Hg),  $\text{Nm}^3 / \text{hr}$ .

All stack emission test results shall be given in dry basis as in 7.1 above, i.e. at zero percent moisture.

*Note : Report the concentration as corrected at 11%  $O_2$*

**Table - 2  
Field Data Sheet**

**Name & Address**

**Date & time of sampling**

**Ambient temperature °C**

**Barometric Pressure (mm mercury column)**

**Moisture in the flue gas (%) flue gas composition (CO<sub>2</sub> %, O<sub>2</sub> %, N<sub>2</sub>)**

**Filter No and weight ( Initial as well as Final)**

| Travers Point | ΔP (mm) | Ts (°K) | Ps | Us (m/s) | Qs (m <sup>3</sup> /hr) | Rs (LPM) | P <sub>m</sub>  |                 | Rm (LPM) | Time (min) | DGM (M <sup>3</sup> ) |       | V <sub>std</sub> (Nm <sup>3</sup> ) |
|---------------|---------|---------|----|----------|-------------------------|----------|-----------------|-----------------|----------|------------|-----------------------|-------|-------------------------------------|
|               |         |         |    |          |                         |          | P <sub>m0</sub> | P <sub>m1</sub> |          |            | Initial               | Final |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |

ΔP = Stack Gas Velocity Pressure, (mm water column), Ts = Stack temperature (°K)

Ps = Static pressure (mm water column), Us = Velocity of stack gas (m/s),

Qs = Volumetric Flow rate / discharge, Rs = Flow at nozzle (LPM),

Pm = Vacuum Pressure Drop (mm mercury column),

Rm = Determination of sampling rate at gas meter. (LPM),

Vstd = Determination of volume of gas sampled

**Other required information:**

- o Feed rate of hazardous waste
- o The nature, composition and quantity of the material being incinerated during monitoring
- o Installed and operating capacity of the incinerator
- o No of sampling ports
- o Internal diameter of the stack
- o Nozzle size selected for sampling
- o Pitot tube constant
- o ID fan capacity
- o Pollution control equipment installed and its status
- o House keeping

**Signature of sample collector**

**Verified by**

**Approved by**

**Occupier/  
Representative of  
the incinerator facility**

**8.0 REFERENCES**

1. Comprehensive Industry Document Series, COINDS/ 20/ 1984 – 85, Central Pollution Control Board
2. EPA Method 5 and Method 17.

# CHAPTER - 2

## Standard Operating Procedure for Particulate Matter Determination

### 1.0 Pre Sampling Activity

Weigh the properly conditioned thimble/filter and place it into the clean, air tight container. Designate appropriate label or ID No. to each thimble/filter container. Follow section 5.4 of part –II (Determination of particulate matter emission from stationary sources) of “Stack Monitoring – Material and Methodology for Isokinetic sampling (method-1).”

Field activity starts with the collection of detail information’s from the industry about the products, raw materials, fuels, and stack dimensions.

### 2.0 Traverse Point Calculation

Calculate the traverse point and accordingly mark the distance from tip of the nozzle, on pitot tube and probe. Do not forget to add the collar length of port to the calculated traverses. For detail calculation see the section 1.3 of “Stack Monitoring Material and Methodology for Isokinetic Sampling (Method-1).

### 3.0 Composition of Flue Gas

Determine flue gas composition by orsat apparatus or multi gas analyzer. In case of Orsat analysis gas sample has to be collected in tedlar bag / non reactive bladder and allowed to cool before analysis. Gas analysis by multi gas analyser may be performed by direct insertion of sampling probe inside the stack and simultaneous estimation of all the components in pre-calibrated gas analyser. At least 3 observations should be taken for average percentile composition. Use gaseous composition data to calculate dry molecular weight of flue gas (Md).

Determine the Dry molecular weight (Md) by following equation

$$Md = 0.44 (\%CO_2) + 0.32 (\% O_2) + 0.28(\% N_2 + \% CO) + \dots\dots$$

### 4.0 Measure ambient temperature (o C) and Barometric pressure in mm Hg.

Ambient Temperature and Barometric pressure readings are to be noted

### 5.0 Check the Leak in Sampling Train

The sampling train after having set up will be tested for leakage by plugging the inlet. The rotameter shall not give a reading beyond 5 lpm when the flow has been set 100 lpm. Also the dry gas meter should give a reading of less than 5 percent of the air flow.



## 6.0 Moisture Determination

Moisture can be determined by condenser method, in principle, involves extracting a sample of the stack gases through a filter for removal of the particulate matter, then through a condenser accumulating the condensate formed in process, and finally through a gas meter. The objective of the test is to collect and measure the volume of all the condensate formed at the condensing temperature from a measured amount of gas. For the detail see the section 1.2 of "Stack Monitoring – Material and Methodology for Isokinetic Sampling (Method-1).

### Calculations

Calculate equivalent vapour of condensate under sampling condition,  $m^3$

$$V_v = \frac{(V_c \times 22.4)}{1000 \times 18} \times \frac{T_M}{273} \times \frac{760}{P_{\text{bar}} - P_m}$$

$V_v$  = Equivalent vapour of condensate under sampling condition,  $m^3$

$V_c$  = Volume of condensate in condensor, ml

$T_m$  = absolute meter temperature,  $^{\circ}K$

$P_m$  = suction at meter, mm mercury column

$P_{\text{bar}}$  = Barometer pressure, mm mercury column

**Calculate the moisture content of the gases using the following equation**

$$B_{wO} = \frac{V_v}{V_v + V_m}$$

$$M = \frac{V_v}{V_v + V_m} \times 100$$

$B_{wO}$  = Proportion by volume of water vapour in stack gas.

$M$  = Moisture in the flue gases, percent

$V_v$  = equivalent vapour volume of condensate under sampling condition.

$V_m$  = Volume of gas sampled ( $m^3$ )

## 7.0 Wet Molecular Weight ( $M_s$ ) Determination

This equation can be used to determine the molecular weight of the stack gas on a wet basis

$$M_s = M_d (1 - B_{wO}) + 18 B_{wO}$$

Md = molecular weight of stack gas on dry basis, / kg - mole

### 8.0 Determine Stack Gas Velocity Pressure ( $\Delta P$ ) And Stack Temperature ( $T_s$ )

- Check and adjust the upper meniscus of manometer fluid at zero.
- Connect +ve and –ve end of the pitot tube in respective points.
- Slowly insert the pitot and thermocouple upto the first traverse mark inside the stack. Keep the positive end towards the direction from which flue is coming. Hold it for stabilisation. Take the reading of fluid displacement in manometer and temperature.
- Repeat the same in next traverse mark and so on.
- Take average reading for  $\Delta P$  and  $T_s$
- For measurement of static gas pressure pitot tube should be rotate by 90 °C from the position of actual  $\Delta P$  measurement. This would provide better accuracy.

### 9.0 Determination of Static Pressure (Absolute Stack Gas Pressure)

For the static pressure determination requires first to disconnect the positive end of the pitot tube then take the reading of velocity pressure at the traverse point in which the calculated average  $\Delta P$  matches closely. For measurement of static gas pressure pitot tube should be rotated by 90° from the position of actual  $\Delta P$  measurement. This would provide better accuracy.

#### Calculate $P_s$

$$P_s = P_{\text{bar}} \pm (\Delta P_s / 13.6)$$

$P_{\text{bar}}$  = Barometric pressure in mm mercury column

$\Delta P_s$  = Stack gas velocity pressure, mm water column

$P_s$  = Static pressure mm Hg column.

Density of Hg = 13.6

### 10.0 Stack Gas Velocity Determination ( $U_s$ )

Connect pitot tube to the stack for velocity determination, calculate the stack gas velocity at all the traverse point by using the following formula. Consider the density factor for correction of velocity pressure and  $\Delta P_s$  to convert water column manometer.

$$U_s = K_p C_p (\Delta P)^{1/2} \left[ \frac{T_s}{(P_s \times M_s)} \right]$$

Where

$U_s$  = stack gas velocity, m/s

$K_p$  = constant

$C_p$  = s-type pitot tube coefficient.

$T_s$  = absolute stack gas temperature, °K

$\Delta P$  = stack gas velocity pressure, mm water column

$P_s$  = absolute stack gas pressure, mm Hg

$M_s$  = molecular weight of stack gas on wet basis, Kg / Kg - mole

### 11.0 Determination of Volumetric Flow Rate/ Discharge

The following equation is used to calculate stack gas volumetric flow rate (m<sup>3</sup> /hr).

$$Q_s = 3600 (U_s) \times A_s (1-B_{wo}) \times \left[ \frac{T_{ref}}{T_s} \right] \left[ \frac{P_s}{P_{ref}} \right]$$

$A_s$  = area of the stack (duct), m<sup>2</sup>

$B_{wo}$  = proportion by volume of water vapour in stack gas.

$T_{ref}$  = 298 °K

$P_{ref}$  = 760 mm

$T_s$  = absolute stack gas temperature, °K

$P_s$  = absolute stack gas pressure

### 12.0 Determination of Flow at Nozzle

Select the nozzle size, in such away that sampling rate a meter shall not exceed 70 % of pump capacity in any case. Cross sectional area of nozzle (mm) for different diameter is as follow

| S No. | Dia of the nozzle (inch) | Cross sectional area (m <sup>2</sup> ) |
|-------|--------------------------|--|
| 1.    | 5/8                      | $1.9783 \times 10^{-4}$                |
| 2.    | 3/4                      | $2.8487 \times 10^{-4}$                |
| 3.    | 1/2                      | $1.2661 \times 10^{-4}$                |
| 4.    | 1/4                      | $3.16531 \times 10^{-5}$               |
| 5.    | 1/8                      | $7.9132 \times 10^{-6}$                |

$$R_s = (U_s \cdot a_n) \cdot 60 \cdot 1000 \text{ LPM}$$

Where,

$R_s$  = sampling rate at nozzle, LPM

$U_s$  = stack gas velocity, m/sec

$A_n$  = area of nozzle,  $m^2$

60 = conversion factor seconds to minute

1000 = conversion factor  $m^3$  to litre

### 13.0 Determination of Sampling Rate at the Gas Meter

The meter for measuring the gas sample measures the gas at conditions of temperature, pressure and moisture content which are different than those in the flue. Therefore, calculate the sampling rate at the gas meter for each sampling points before starting the test and record on the log the required rate (Table 1). Calculate the sampling rate at the gas meter as follows:

$$R_m = R_s \times \frac{T_s}{T_m} \times \frac{P_{bar} - P_s}{P_{bar} - P_m} \times \frac{V_m}{V_m + V_v}$$

$R_m$  = Flow rate through meter,  $m^3/s$

$R_s$  = Sampling rate at nozzle, LPM

$T_m$  = Temperature at metering condition,  $^{\circ}K$

$T_s$  = Absolute stack gas temperature,  $^{\circ}K$

$P_s$  = Absolute stack gas pressure, mm mercury column

$P_{bar}$  = Barometer pressure, mm mercury column

$P_m$  =  $(P_{m1} - P_{m0}) / 2$  Suction at meter, mm mercury column

$V_m$  = Volume of gas sampled at meter conditions,  $m^3$

$V_v$  = Equivalent vapour volume of condensate at meter conditions,  $m^3$

*Note: Take initial reading of vacuum gauge ( $P_{m0}$ ) in mm Hg at the starting of sampling and final vacuum pressure ( $P_{m1}$ ) in mm Hg just before putting off the pump when sampling is complete. Calculate average difference in suction pressure, referred as  $P_m$*

### 14.0 Sampling

Start the test after the sampling rate has been calculated and train assembled and checked for leakages. When equipment is ready in all respect, record the initial dry gas

meter reading and push the sampling probe carefully into the duct to the point nearest to the back wall. Take the sample appropriately as per the requirement and with all the necessary precaution.

### 15.0 Determination of Volume of Gas Sampled

Calculate the volume of gas sampled using the following equation:

$$R_{std} = V_m Y \frac{P_{bar} - P_m}{760 \text{ mm Hg}} \times \frac{273 + 25 \text{ }^\circ\text{C}}{T_m + 273}$$

$T_m$  = Temperature of gas at dry meter condition,  $^\circ\text{C}$

$V_m$  = Volume of gas sampled at dry gas meter conditions,  $\text{m}^3$

$(P_{bar}-P_m)$  = Actual pressure in sampling train, mm mercury column.

$P_m$  = Static pressure in sampling train, mm mercury column.

$P_{bar}$  = Barometric pressure in sampling train, mm mercury column.

$Y$  = Calibration factor of dry gas meter.

### 16.0 Sample Recovery

After the sampler has cooled, brush down the dust on the side of the nozzle carefully into the thimble using a small brush remove the thimble and replace it in same labeled container. In the case of filter holder is kept outside during the sampling, the dust from the sampling probe before the filter holder should be brushed down into the filter.

#### Note:

*See the section 6.0 of part –II (Determination of particulate matter emission from stationary sources) of “Stack Monitoring – Material and Methodology for Isokinetic Sampling (method-1).”*

### 17.0 Determination of Dust Concentration

Determine the mass of dust collected in the thimble by difference i.e weighing the thimble before and after the run. Dry the thimble in an oven for about 2 hours at  $120 \text{ }^\circ\text{C}$  prior to sampling. After sampling, cool, dry and again weigh the thimble along with dust maintaining the same condition as prior to sampling.

**Calculate the dust concentration using the following equation:**

$$\text{Dust Concentration in mg /Nm}^3 \text{ (25 }^\circ\text{C, 760 mm Hg, dry basis)} = \frac{(W_2 - W_1) \text{ gm} \times 1000}{V_{std}}$$

$V_{std}$  = Volume of dry gas through the meter  
(25 °C, 760 mm Hg), Nm<sup>3</sup>

$W_1$  = Initial weight of filter paper

$W_2$  = Final weight of filter paper

### 18.0 Correction of the result at 11 % O<sub>2</sub>

O<sub>2</sub> correction is only carried out, if O<sub>2</sub> corrections > 11%. For O<sub>2</sub> < 11% no correction is allowed.

It's require to correct the value for the 11% O<sub>2</sub> by following formula

$$E_s = \frac{21 - O_s}{21 - O_m} \times E_M$$

$E_s$  = Calculated emission concentration at the standard percentage oxygen concentration

$E_M$  = Measured emission concentration

$O_s$  = Standard oxygen concentration

$O_M$  = Measured oxygen concentration

### 19.0 Determination of Emission Rate

Calculate the dust emission rate as following

$$\text{Dust Emission Rate (Kg/Hr)} = \frac{E_m \times Q_s}{10^6}$$

$Q_s$  = Flue gas flow rate (25 °C, 760 Hg mm Hg), Nm<sup>3</sup>/hr.

Note: Report the concentration as corrected at 11% O<sub>2</sub>

**Table - 1**  
**Field Data Sheet**

**Name & Address**

**Date & time of sampling**

**Ambient temperature °C**

**Barometric Pressure (mm mercury column)**

**Moisture in the flue gas (%) flue gas composition (CO<sub>2</sub> %, O<sub>2</sub> %, N<sub>2</sub>)**

**Filter No and weight ( Initial as well as Final)**

| Travers Point | ΔP (mm) | Ts (°K) | Ps | Us (m/s) | Qs (m <sup>3</sup> /hr) | Rs (LPM) | P <sub>m</sub>  |                 | Rm (LPM) | Time (min) | DGM (M <sup>3</sup> ) |       | V <sub>std</sub> (Nm <sup>3</sup> ) |
|---------------|---------|---------|----|----------|-------------------------|----------|-----------------|-----------------|----------|------------|-----------------------|-------|-------------------------------------|
|               |         |         |    |          |                         |          | P <sub>m0</sub> | P <sub>m1</sub> |          |            | Initial               | Final |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |

ΔP = Stack Gas Velocity Pressure, (mm water column), Ts = Stack temperature (°K)

Ps = Static pressure (mm water column), Us = Velocity of stack gas (m/s),

Qs = Volumetric Flow rate / discharge, Rs = Flow at nozzle (LPM),

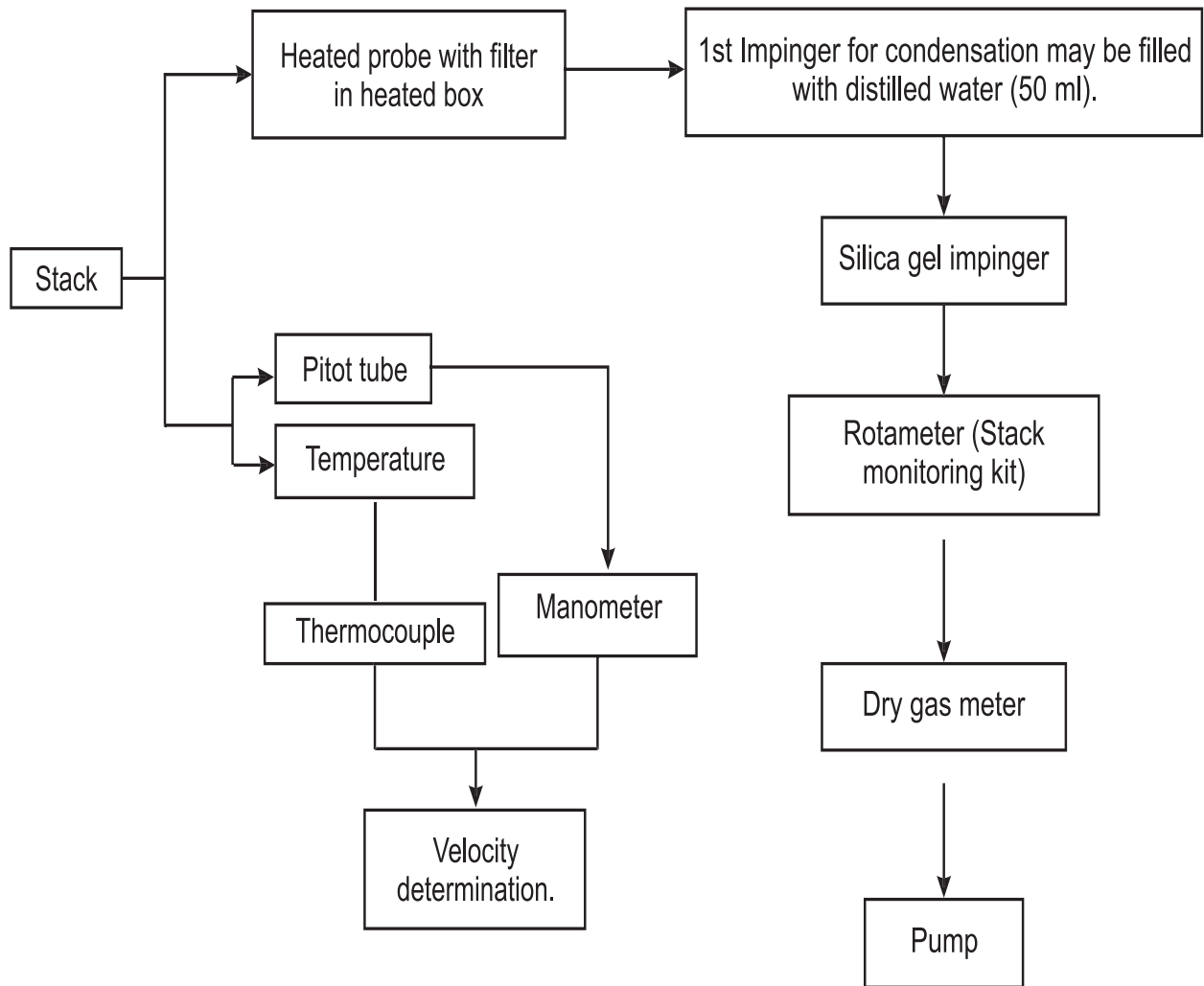
Pm = Vacuum Pressure Drop (mm mercury column),

Rm = Determination of sampling rate at gas meter. (LPM),

Vstd = Determination of volume of gas sampled

**Other required information:**

- o Feed rate of hazardous waste
- o The nature, composition and quantity of the material being incinerated during monitoring
- o Installed and operating capacity of the incinerator
- o No of sampling ports
- o Internal diameter of the stack
- o Nozzle size selected for sampling
- o Pitot tube constant
- o ID fan capacity
- o Pollution control equipment installed and its status
- o House keeping



**Fig 1 : Sampling train for Particulate Matter**



### DETERMINATION OF HYDROGEN HALIDES (Hx) and HALOGENS IN SOURCE EMISSION

#### ( Part- I)

#### 1.0 PRINCIPLE

Gaseous and particulate pollutants are withdrawn isokinetically from the source and collected in an optional cyclone, preferably on a PTFE filter, and in absorbing solutions. The cyclone collects any liquid droplets and is not necessary if the source emissions do not contain them; however, it is preferable to include the cyclone in the sampling train to protect the filter from any moisture present. The filter collects other particulate matter including halide salts. Acidic and alkaline absorbing solutions collect the gaseous hydrogen halides and halogens, respectively. Following sampling for emissions containing liquid droplets, any halides/halogens dissolved in the liquid in the cyclone and on the filter are vaporized to gas and collected in the impingers by pulling conditioned ambient air through the sampling train. The hydrogen halides are solubilized in the acidic solution and form chloride (Cl<sup>-</sup>), bromide (Br<sup>-</sup>), and fluoride (F<sup>-</sup>) ions. The halogens have a very low solubility in the acidic solution and pass through to the alkaline solution where they are hydrolyzed to form a proton (H<sup>+</sup>), the halide ion, and the hypohalous acid (HClO or HBrO). Sodium thiosulfate is added in excess to the alkaline solution to assure reaction with the hypohalous acid to form a second halide ion such that two halide ions are formed for each molecule of halogen gas. The halide ions in the separate solutions are measured by ion chromatography (IC).

#### 2.0 APPLICABILITY

This method is applicable for determining emissions of hydrogen halides (HX) [hydrogen chloride (HCl), hydrogen bromide (HBr), and hydrogen fluoride (HF)] and halogens [chlorine (Cl<sub>2</sub> and bromine (Br)] from stationary sources. Same method may be applicable for those sources, which are controlled by wet scrubbers and emit acid particulate matter. Due to corrosive nature of expected flue gas glass lined probe is recommended for this method.

#### 2.1 DETECTION LIMIT

The in-stack detection limit is approximately 0.05 μg per liter of stack gas; the analytical detection limit is 0.1 μg/ml.

#### 3.0 INTERFERENCES

Volatile materials, such as chlorine dioxide (ClO<sub>2</sub>) and ammonium chloride (NH<sub>4</sub>Cl), which produce halide ions upon dissolution during sampling, are potential interferents. Interferents for the halide measurements are the halogen gases which disproportionate to a hydrogen halide and a hydrohalous acid upon dissolution in water. However, the use of acidic rather than neutral or basic solutions for collection of the hydrogen halides greatly reduces the dissolution of any halogens passing through this solution. The simultaneous presence of

HBr and Cl<sub>2</sub> may cause a positive bias in the HCl result with a corresponding negative bias in Cl<sub>2</sub> result as well as affecting the HBr / Br split. . High concentrations of nitrogen oxides (NO<sub>x</sub>) may produce sufficient nitrate (NO<sub>3</sub>) to interfere with measurement of very low Br- levels.

#### 4.0 REAGENTS

##### 4.1 Sampling Reagents

**Table 1 : Sampling reagents**

| S.No | Reagents   | Procedure for preparation  |
|------|--|--|
| 1    | Deionized, distilled water   |  |
| 2    | 0.1 N Sulfuric Acid (H <sub>2</sub> SO <sub>4</sub> )  | To prepare 100 ml of the absorbing solution for the front impinger pair, slowly add 0.28 ml of concentrated H <sub>2</sub> SO <sub>4</sub> to about 90 ml of water while stirring, and adjust the final volume to 100 ml using additional water. Shake well to mix the solution. |
| 3    | 0.1 N Sodium Hydroxide (NaOH.  | To prepare 100 ml of the alkaline absorbing solution for the fourth impinger, dissolve 0.40 g of solid NaOH in about 90 ml of water, and adjust the final solution volume to 100 ml using additional water. Shake well to mix the solution.                                      |
| 4    | Sodium Thiosulfate (Na <sub>2</sub> S <sub>2</sub> O <sub>3</sub> . 5H <sub>2</sub> O) powder. |  |

##### 4.2 Analytical Reagents

- Deionised / nano pure distilled water
- Absorbing Solution Blanks
- Stock Standard Solutions

#### 5.0 SAMPLING

##### 5.1 Preparation of Collection Train

**Prepare the sampling train as following:**

Pour 50 ml of the acidic absorbing solution into each one of the first pair of impingers, and 50 ml of the alkaline absorbing solution into each one of the second pair of impingers. Connect the impingers in series with the knockout impinger first, if used, followed by the two impingers containing the acidic absorbing solution and the two impingers containing the alkaline absorbing solution. Place a fresh charge of silica gel, or equivalent, in the drying tube or impinger (after

the one more empty impinger) at the end of the impinger train. Adjust the probe temperature and the temperature of the filter and the stopcock, i.e., the heated area in Figure – 1 to a temperature sufficient to prevent water condensation. This temperature should be at least 20 °C above the source temperature, but not greater than 120 °C. The temperature should be monitored throughout run to ensure that the desired temperature is maintained.

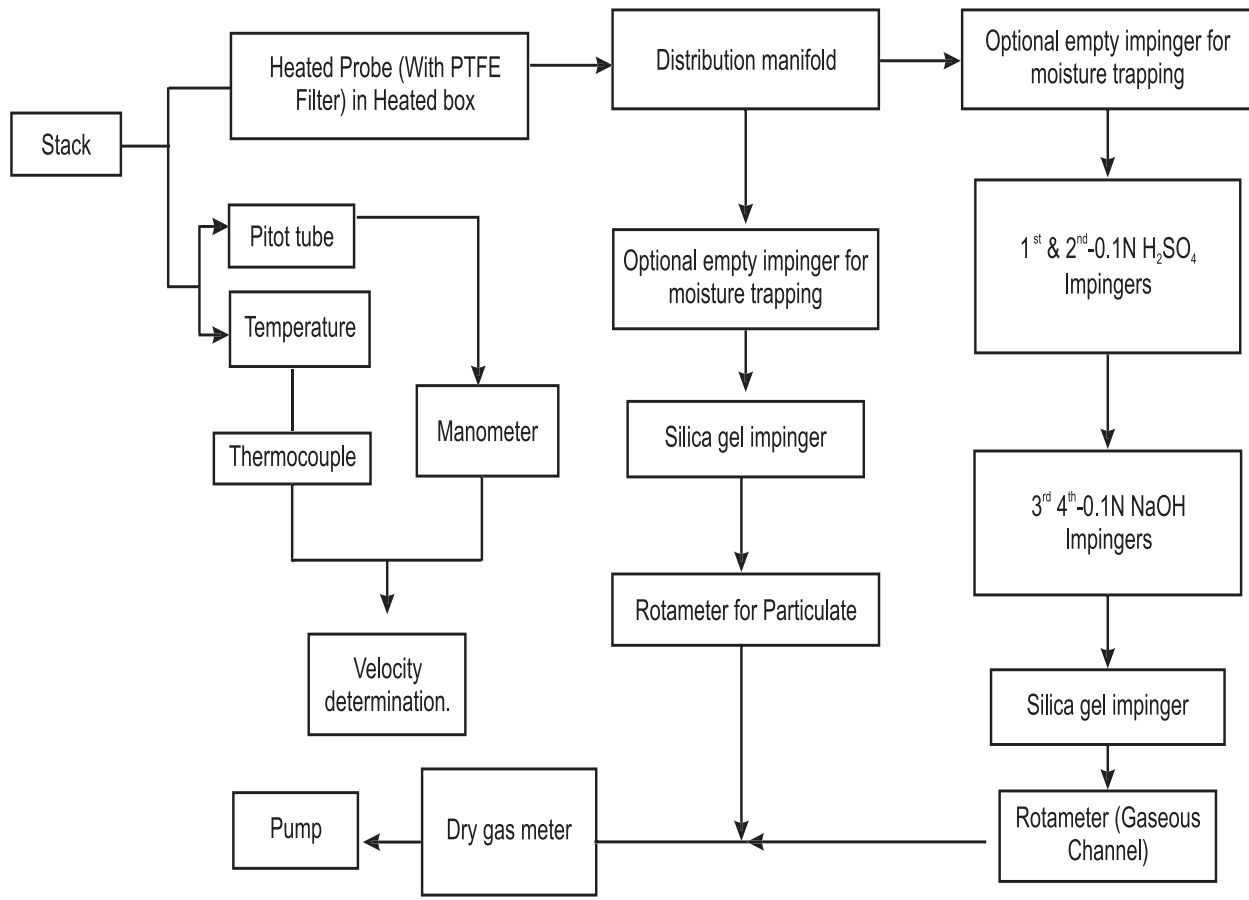


Fig - 1: Intergrated Sampling train for particulate and gaseous H<sub>x</sub> and Halogens

### 5.1.1 Leak-check procedure

The sampling train after having set up will be tested for leakage by plugging the inlet. The rotameter shall not give a reading beyond 5 lpm when the flow has been set 100 lpm. Also the dry gas meter should give a reading of less than 5 percent of the air flow.

### 5.1.2 Preliminary determinations and isokinetic sampling

Determine the stack pressure, temperature, leak check, calculation of Isokinetic velocity, volumetric flow rate, flow at nozzle/ selection of nozzle, adjustment of flow rate at rotameter, temperature at metering point and volume of gas sampled, pressure drop during sampling.

Note:

*For the Calculation of isokinetic velocity and collection of the sample refer Method -1 "Stack monitoring – Material and Methodology for Isokinetic Sampling" or SOP for the particulate matter determination*

### **5.1.3 Sample collection**

Turn on the vacuum pump and make a slight vacuum of 25 mm Hg (1 in. Hg). Set the sampling rate in gaseous train at 2 LPM & allow rest of the flow for isokinetic sampling rate in particulate train and maintain this rate to within 10 percent during the entire sampling run. Take readings of the dry gas meter volume and temperature, rate meter, and vacuum gauge at least once every five minutes during the run. A sampling time of one hour is recommended. Shorter sampling times may introduce a significant negative bias in the HCl concentration. During calculation of volume of air passes through the impinger & filter should be done by adding both the flow rate multiplied by sampling time. At the conclusion of the sampling run, remove the train from the stack and cool it.

### **5.2 Sample Recovery**

Collect filter separately. No heating should be done in conditioning of filter preferably desiccation or use of conditioning room is suggested for Pre-conditioning and post-conditioning of filter. Disconnect the impingers after sampling. Quantitatively transfer the contents of the acid impingers and the knockout impinger, if used, to a leak-free storage bottle. Add the water rinses of each of these impingers and connecting glassware to the storage bottle. Quantity rinsing water should not be used more than 25ml. Repeat this procedure for the alkaline impingers and connecting glassware using a separate storage bottle. Add 25 mg sodium thiosulfate to ensure complete reaction with the hypohalous acid to form a second Cl<sup>-</sup> ion in the alkaline solution. Save portions of the absorbing reagents (0.1 N H<sub>2</sub>SO<sub>4</sub> and 0.1 N NaOH) equivalent to the amount used in the sampling train dilute to the approximate volume of the corresponding samples using rinse water directly from the wash bottle being used. Add the same (25 mg) amount of sodium thiosulfate solution to the 0.1 N NaOH absorbing solution blank. Also, save a portion of the rinse water used to rinse the sampling train. Place each in a separate, pre-labeled storage bottle. The sample storage bottles should be sealed, shaken to mix, and labeled. Mark the fluid level.

### **5.3 Sample Preparation for Analysis**

Note the liquid levels in the storage bottles and confirm on the analysis sheet whether or not leakage occurred during transport. If major leakage is observed make up with DI water upto the marked level. Quantitatively (the whole sample or aliquot) transfer the sample solutions to 100-ml volumetric flasks, and dilute to 100 ml with water.

For acid mists extract the ions from thimble with 50 ml distilled water under ultrasonic bath at 60 °C for 1 hour.

## 6.0 SAMPLE ANALYSIS

- All the samples extracted mists and impingers (first 2 – acidic and last two alkaline) should be analyzed separately for target ions.
- Analysis of the acid and alkaline absorbing solution samples requires separate standard calibration curves if test run does not conform proper separation and baseline artifacts.
- Ensure adequate baseline separation of the analyses. Before sample analysis, establish a stable baseline. Next, inject a sample of water and determine if any Cl<sup>-</sup>, Br<sup>-</sup>, or F<sup>-</sup> appears in the chromatogram. If any of these ions are present, repeat the load/injection procedure until they are no longer present.
- Between injections of the appropriate series of calibration standards reagent blanks, quality control sample, and the field samples should be injected. Duplicate injections are recommended and use the mean response to determine the concentrations of the field samples and reagent blanks using the linear calibration curve (forced through zero or linear quadratic). The values from duplicate injections should agree within 5 percent of their mean for the analysis to be valid. Dilute any sample and the blank with equal volumes of water if the concentration exceeds that of the highest standard.

## 7.0 CALCULATIONS

Retain at least one extra decimal figure beyond those contained in the available data in intermediate calculations, and round off only the final answer appropriately. As the individual analysis is performed for mist, acidic sample and alkaline sample in this method, individually calculated concentrations should be sum up to report final concentration of target analytes in flue gas. The formulae for individual calculation are stated below.

### 7.1 Sample Volume, Dry Basis, Corrected to Standard Conditions

$$V_{mstd} = V_m \cdot Y \left[ \frac{T_{std}}{T_m} \right] \left[ \frac{P_{bar}}{P_{std}} \right] = K_1 \cdot Y \cdot V_m \left[ \frac{P_{bar}}{P_m} \right]$$

Where:

$K_1$  = 0.3858 °K/mm Hg for metric units,

= 17.64 °C/in. Hg for English units

$P_{bar}$  = Barometric pressure at the exit orifice of the DGM, mm Hg (in. Hg).

$P_{std}$  = Standard absolute pressure, 760 mm Hg (29.92 in.Hg).

$T_m$  = Average DGM absolute temperature, °K (°C).

$T_{std}$  = Standard absolute temperature, 293 °K

$Y$  = Dry gas meter calibration factor

$V_{m(std)}$  = Dry gas volume measured by the dry gas meter, corrected to standard conditions, Nm<sup>3</sup>

$V_m$  = {Sampling rate in gas channel (LPM) X duration (Minutes)} / 1000 m<sup>3</sup>.

**Table - 1  
Field Data Sheet**

**Name & Address**  
**Date & time of sampling**  
**Ambient temperature °C**  
**Barometric Pressure (mm mercury column)**  
**Moisture in the flue gas (%) flue gas composition (CO<sub>2</sub> %, O<sub>2</sub> %,N<sub>2</sub>)**  
**Filter No and weight ( Initial as well as Final)**

| Travers Point | ΔP (mm) | Ts (°K) | Ps | Us (m/s) | Qs (m <sup>3</sup> /hr) | Rs (LPM) | P <sub>m</sub>  |                 | Rm (LPM) | Time (min) | DGM (M <sup>3</sup> ) |       | V <sub>std</sub> (Nm <sup>3</sup> ) |
|---------------|---------|---------|----|----------|-------------------------|----------|-----------------|-----------------|----------|------------|-----------------------|-------|-------------------------------------|
|               |         |         |    |          |                         |          | P <sub>m0</sub> | P <sub>m1</sub> |          |            | Initial               | Final |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |

ΔP = Stack Gas Velocity Pressure, (mm water column), Ts = Stack temperature (°K)  
Ps = Static pressure (mm water column), Us = Velocity of stack gas (m/s),  
Qs = Volumetric Flow rate / discharge, Rs = Flow at nozzle (LPM),  
Pm = Vacuum Pressure Drop (mm mercury column),  
Rm = Determination of sampling rate at gas meter. (LPM),  
Vstd = Determination of volume of gas sampled

**Other required information:**

- o Feed rate of hazardous waste
- o The nature, composition and quantity of the material being incinerated during monitoring
- o Installed and operating capacity of the incinerator
- o No of sampling ports
- o Internal diameter of the stack
- o Nozzle size selected for sampling
- o Pitot tube constant
- o ID fan capacity
- o Pollution control equipment installed and its status
- o House keeping

**Signature of sample collector**      **Verified by**      **Approved by**      **Occupier/  
Representative of  
the incinerator facility**

## Analysis of Hx and Halogens

### (Part – II)

#### 1.0 PURPOSE AND APPLICABILITY

This document outlines procedures for the filter preparation and extraction, and the subsequent determination of anions in filter extracts.

#### 2.0 SUMMARY OF METHOD

Teflon filters for collection of anions do not require pretreatment. Exposed filter samples are extracted by a method appropriate for the analyte(s) of interest. Filters are extracted with deionized water. Extraction with deionized water makes it possible to analyze for both anions and cations. Sample extracts are passed through a column of ion chromatographic resin consisting of polymer beads coated with quaternary ammonium active sites. During passage through the column, anion separation occurs due to the different affinities of the anions for the active resin sites. Following separation, the anions pass through a suppressor column which exchanges all cations for H<sup>+</sup> ions. An eluent, which yields a low conducting acid, is used. Species are detected and quantified as their acids (e.g., HCl) by a conductivity meter

#### 3.0 INTERFERENCES

Large amounts of anions eluting close to the ions of interest will result in interference. No interferences have been observed in Teflon / nylon filters samples analyzed. If interferences are observed, several steps to increase separation can be taken, such as reducing eluent strength and/or flow rate or replacing the columns.

#### 4.0 APPARATUS AND MATERIALS

- Filters (Teflon/Nylon)
- Volumetric flask, 1000 mL, 500 mL, 250 mL, 100 mL and 50 mL
- Tweezers
- Glass rod drying racks
- Tweezers
- Adjustable Eppendorf or equivalent micro-pipettes
- Ultrasonic bath
- Syringe filter with 13 mm Nylon filter holder and filter discs
- 250 mL glass beakers



## Reagents

Stock Standards:- Use high purity graded chemicals for the preparation of all solutions. Dry chemicals used for the preparation of calibration standards at 105 °C for 2 hours and cool in desiccators immediately before weighing. The stock solutions containing (anion) = 1000 mg/L can also be prepared by dissolving the appropriate amount of a suitable salt (purity standard.) in ultrapure water. The sample weight required per liter ultrapure water is shown in the Table 1. To prepare the anion standard, these stock solutions are then diluted to the desired concentrations with ultrapure water.

**Table 1 : Required weight of salts to prepare 1000 ppm stock individual standards**

| Anions   | Salt | Weights in (g) | Final Volume | Concentrations |
|----------|------|----------------|--------------|----------------|
| Fluoride | NaF  | 2.2100         | 1000 mL      | 1000 mg/L      |
| Chloride | NaCl | 1.6484         | 1000 mL      | 1000 mg/L      |
| Bromide  | NaBr | 1.4998         | 1000 mL      | 1000 mg/L      |

Commercially available high purity individual liquid stock standards (1000 ppm) are also useful. Mix standards should be chosen carefully considering the difference in responses of individual ions in a chromatogram.

### Calibration Standards preparation:

Prepare Standard Mix - A solution containing 100 ppm each Cl<sup>-</sup>, from 1000 ppm stock by diluting the same.

Prepare Standard Mix – B solution containing F<sup>-</sup> (5 ppm) and 20 ppm Br by diluting the respective stock. Final calibration standards for 6 levels are prepared following the Table given 2. Prepare fresh working calibration standards weekly and refrigerate when not in use. Stock Standards may be used for 6 months if refrigerated properly.

**Table 2 : Calibration Standards preparation guidelines (Final volume 100 ml)**

| Ions     | Level I            | Level II        | Level III       | Level IV        | Level V           | Level VI          |
|----------|--------------------|-----------------|-----------------|-----------------|-------------------|-------------------|
|          | 0.5ml A + 0.5 mL B | 1 ml A + 1 mL B | 2 ml A + 2 mL B | 5 ml A + 5 mL B | 10 ml A + 10 mL B | 15 ml A + 15 mL B |
| Fluoride | 0.025              | 0.05            | 0.1             | 0.25            | 0.5               | 1.0               |
| Chloride | 0.5                | 1.0             | 2.0             | 5.0             | 15.0              | 15.0              |
| Bromide  | 0.1                | 0.2             | 0.4             | 1.0             | 3.0               | 3.0               |



**Eluent:**

It is specific for brand and make to instrument and columns being used. For concentration and composition of eluent please refer to the application notes. Generally for anion analysis  $\text{NaHCO}_3$  -  $\text{Na}_2\text{CO}_3$  eluent is used. Eluents are prepared by dissolving prescribed amount of chemicals in high purity nano-pure distilled water. Eluents are required to be filtered through  $0.22 \mu\text{m}$  nylon filter.

**Suppressor:**

Dionex system has inbuilt ionic suppressor system but Metrohm system chemical suppression for anions with 2.8 mL concentrated (98%) pure  $\text{H}_2\text{SO}_4$  diluted in 1 liter is used for regeneration of suppressor cartridges. Pure water (DI) is used for washing of suppressor during run.

**5.0 SAMPLE HANDLING**

Laboratory shall provide chain-of-custody documentation with all sample shipments to track and ensure that filter samples are collected, transferred, stored, and analyzed by authorized personnel; sample integrity is maintained during all phases of sample handling and analysis; and an accurate written record is maintained of sample handling and treatment from the time of its collection, through the laboratory analytical process, to the eventual relinquishing of all data to the project coordinator.

**Filter / Thimble Extraction Procedure**

Filters to be analyzed for halides are extracted with water. Extraction with deionized water makes it possible to analyze for these ions.

- i) Remove filters to be extracted from the freezer and allow them to equilibrate to room temperature.
- ii) Using gloved hands and tweezers, place each filter in cleaned glass beakers (250mL) that has been labeled with the sample I.D.
- iii) Add measured 50-100 mL of deionized water. The extraction volume will depend upon the quantity of dust accumulated on filter paper.
- iv) Place the batch of beakers in ultrasonic bath, expose them to ultrasonic energy in a bath for 60 minutes at  $60^\circ\text{C}$ , and then allow them to sit at room temperature overnight. Refrigerate at least one additional night prior to analysis.
- v) Record the date of extraction on the Sample Filter Processing Form. Allow the samples to warm to room temperature just prior to analysis.

- vi) Filter all the samples by syringe filter using 13 mm 6.6  $\mu\text{m}$  nylon filter disc. Ensure no particle should pass through in samples to be injected. Injection may be done manually or through auto sampler.

### **The liquid sample (alkaline and acidic) analysis**

The alkaline and acidic samples are injected separately in IC system and analyzed for all the three halides.

*Note: Different calibration curve for acidic and alkaline analysis may be required to get better baseline separation in IC system. In this case separate set of calibration Standards in two different absorbing media shall be prepared*

#### **IC Procedure:**

- i) Fill the eluent reservoirs with the eluent.
- ii) Fill the suppressor reservoir and distilled water reservoir in case of chemical suppression technique (Metrohm instrument)
- iii) Start the eluent flow, activate the self-regenerating suppressor in case of (Dionex instrument), and allow the baseline to stabilize.
- iv) In case of Metrohm instrument ensure that all the three suppressor cartridge are recharged. Start baseline determination wait until stable baseline is achieved.
- v) Inject two pure distilled water blanks to flush the system and to ensure that the system is operating properly.
- vi) Using the calibration schedule, perform the monthly multipoint calibration over the range.
- vii) Inject middle level calibration standards daily to know the status of performance. If the observed value for any ion differs by more than 10 percent from the known values, identify and correct the problem before analyzing samples.
- viii) Load the sample extracts into the autosampler vials according to the schedule prepared for that day. Typically, fifty field samples are analyzed per day. The daily schedule includes, at a minimum, 3 duplicate samples, 2 spiked samples and 5 QA/QC samples.
- ix) Begin the analysis run, occasionally checking to ensure that the system is operating properly.
- x) Examine the data at the end of the run. If the concentration of any ion exceeds the upper end of the calibration curve, dilute the sample appropriately and include with the samples to be analyzed the following day.

## 6.0 CALCULATIONS AND DATA REDUCTION

In-built software will always give some results, which may not be acceptable all the time. Study each and every chromatogram and perform manual integration of peaks if necessary. Proceed to report format and copy the results in Excel data sheet.

$$m_{HX} = K (Vs) (Sx-Bx)$$

Where

$m_{HX}$  = Mass of HCl, HBr, or HF in sample,  $\mu\text{g}$ .

$B_x$  = Mass concentration of applicable absorbing solution blank,  $\mu\text{g}$  halide ion ( $\text{Cl}^-$ ,  $\text{Br}^-$ ,  $\text{F}^-$ ) / ml, not to exceed 1  $\mu\text{g}/\text{ml}$  which is 10 times the published analytical detection limit of 0.1  $\mu\text{g}/\text{ml}$ .

$S_x$  = Analysis of sample,  $\mu\text{g}$  halide ion ( $\text{Cl}^-$ ,  $\text{Br}^-$ ,  $\text{F}^-$ ) / ml

$V_s$  = Volume of filtered and diluted sample, ml.

$K_{\text{HCl}}$  = 1.028 ( $\mu\text{g}$  HCl /  $\mu\text{g}$ -mole) / ( $\mu\text{g}$   $\text{Cl}^-$  /  $\mu\text{g}$ -mole).

$K_{\text{HBr}}$  = 1.013 ( $\mu\text{g}$  HBr /  $\mu\text{g}$ -mole) / ( $\mu\text{g}$   $\text{Br}^-$  /  $\mu\text{g}$ -mole).

$K_{\text{HF}}$  = 1.053 ( $\mu\text{g}$  HF /  $\mu\text{g}$ -mole) / ( $\mu\text{g}$   $\text{F}^-$  /  $\mu\text{g}$ -mole).

## 6.2 Total $\mu\text{g}$ $\text{Cl}^-$ , $\text{Br}^-$ , $\text{F}^-$ per Sample

Where

$M_{x2}$  = Mass of  $\text{Cl}^-$ ,  $\text{Br}^-$  or in sample,  $\mu\text{g}$ .

$B_x$  = Mass concentration of applicable absorbing solution blank,  $\mu\text{g}$  halide ion ( $\text{Cl}^-$ ,  $\text{Br}^-$ ,  $\text{F}^-$ ) / ml, not to exceed 1  $\mu\text{g}/\text{ml}$  which is 10 times the published analytical detection limit of 0.1  $\mu\text{g}/\text{ml}$ .

$S_x$  = Analysis of sample,  $\mu\text{g}$  halide ion ( $\text{Cl}^-$ ,  $\text{Br}^-$ ,  $\text{F}^-$ ) / ml

$V_s$  = Volume of filtered and diluted sample, ml.

Calculated values for all the aliquots (Thimble, Alkaline trap and acidic trap) are sum up and the total mass is divided by standardised Air volume to get respective concentrations in  $\text{mg}/\text{Nm}^3$ .

Hence, for F,  $\text{Cl}_2$  or  $\text{Br}_2$

$$C_x = [\{m_{x2(\text{Thimble})} + m_{x2(\text{Alkaline trap})} + m_{x2(\text{Acidic Trap})}\} * 10^{-3}] / V_{m(\text{std})} \text{ mg}/\text{Nm}^3$$

Where,

$C_x$  = Concentration of  $\text{Cl}^-$ ,  $\text{Br}^-$ ,  $\text{F}^-$  in Flue gas

$m_{x2}$  = Mass of  $Cl^-$ ,  $Br^-$ , or  $F^-$  in sample ( $\mu g$ ) in respective aliquot.

$V_{m(std)}$  = Dry gas volume measured by the DGM, corrected to standard conditions,  $Nm^3$

Hence, for HCl, HBr, or HF

$$C_{HX} = [\{m_{HX (Thimble)} + m_{HX (Alkaline trap)} + m_{HX (Acidic Trap)}\} * 10^{-3}] / V_{m(std)} \text{ mg}/Nm^3$$

Where,

$C_{HX}$  = Concentration of HCl, HBr or HF in flue gas.

$m_{HX}$  = Mass of HCl, HBr or HF in sample ( $\mu g$ ) in respective aliquot.

$V_{m(std)}$  = Dry gas volume measured by the DGM, corrected to standard conditions,  $Nm^3$

*Note: Report the concentration as corrected at 11%  $O_2$  (as mentioned in the method for PM determination)*

## 7.0 QUALITY ASSURANCE AND QUALITY CONTROL

The analyst should be familiar with the terms and use of following parameters for QA/QC

### **Blank:**

a sample that has not been exposed to the analyzed sample stream in order to monitor contamination during sampling, transport, storage or analysis. The blank is subjected to the usual analytical and measurement process to establish a zero baseline or background value and is sometimes used to adjust or correct routine analytical results.

### **Field Blanks:**

These are filters that are treated in all ways as a normal sample (including installation on the sampler) except that no air is sampled on them. (These are also referred to as equipment blanks in LIMS.)

### **Continuing Calibration Blank (CCB):**

A "zero" standard analyzed along with the CCV standard to verify that the lower end of the calibration curve remains valid during the analysis of the batch of samples. A CCB is analyzed at the beginning of each batch, at the end of a batch, and at least every 20 samples during a batch.

### **Continuing Calibration Verification Standard (CCV):**

A standard analyzed after the initial calibration to verify that the instrument calibration remains valid. The concentration of this standard is varied over the calibration range during each run. A CCV is analyzed at the beginning of each batch, at the end of a batch, and at least every 20 samples during a batch.

**Laboratory Duplicate:**

Aliquots of a sample taken from the same container under laboratory conditions and processed and analyzed independently. In this SOP, laboratory duplicates are created by extracting equal portions of the loaded filters.

**Matrix Spike (spiked sample or fortified sample):**

A sample prepared by adding a known mass of target analyte to a specified amount of matrix sample for which an independent estimate of Target analyte concentration is available. Matrix spikes are used, for example, to determine the effect of the matrix on a method's recovery efficiency. In this SOP, a matrix spike consists of adding a known concentration of analyte(s) to a separate aliquot of the filter.

**Method Detection Limit (MDL):**

The minimum concentration of an analyte that can be identified, measured, and reported with 99% confidence that the analyte concentration is greater than zero.

**Method Reporting Limit (MRL):**

The minimum concentration of an analyte that is reported. Generally, this will be 3 to 5 times the concentration of the MDL.

If correlation coefficient for all the multipoint calibration curves does not exceed 0.998, stop the analysis and identify the problem.

Analyze QC samples at the beginning of every analytical run. Compare the results with those obtained during previous QC tests. If the observed concentration of any ion differs from the known value by greater than 10%, stop the analysis until the problem is identified and corrected. Analyze a duplicate sample, a QA/QC sample, and a spiked sample after at least every 20 field samples.

**8.0 REFERENCES**

1. DRI Document No. 8068.1F4, Appendix D, Section 4.2
2. Steinsberger, S. C. and J. H. Margeson, "Laboratory and Field Evaluation of a Methodology for Determination of Hydrogen Chloride Emissions from Municipal and Hazardous Waste Incinerators," U.S. Environmental Protection Agency, Office of Research and Development, Report No. 600/3- 89/064, April 1989. Available from the National Technical Information Service, Springfield, VA 22161 as PB89220586/AS.
3. State of California, Air Resources Board, Method 421, "Determination of Hydrochloric Acid Emissions from Stationary Sources," March 18, 1987. 3. Cheney, J.L. and

- C.R. Fortune. Improvements in the Methodology for Measuring Hydrochloric Acid in Combustion Source Emissions. *J. Environ. Sci. Health.* A19(3): 337-350. 1984.
4. Stern, D. A., B. M. Myatt, J. F. Lachowski, and K. T. McGregor. Speciation of Halogen and Hydrogen Halide Compounds in Gaseous Emissions. In: *Incineration and Treatment of Hazardous Waste: Proceedings of the 9th Annual Research Symposium*, Cincinnati, Ohio, May 2-4, 1983. Publication No. 600/9- 84-015. July 1984. Available from National Technical Information Service, Springfield, VA 22161 as PB84-234525.
  5. Holm, R. D. and S. A. Barksdale. Analysis of Anions in Combustion Products. In: *Ion Chromatographic Analysis of Environmental Pollutants*. E. Sawicki, J. D. Mulik, and E. Wittgenstein (eds.) Ann Arbor, Michigan, Ann Arbor Science Publishers. 1978. pp. 99-110.
  6. Steinsberger, S. C. and J. H. Margeson. Laboratory and Field Evaluation of a Methodology for Determination of Hydrogen Chloride Emissions from Municipal and Hazardous Waste Incinerators. U.S. Environmental Protection Agency, Office of Research and Development. Publication No. 600/3-89/064. April 1989. Available from National Technical Information Service, Springfield, VA 22161 as PB89220586/AS.
  7. State of California Air Resources Board. Method 421 - Determination of Hydrochloric Acid Emissions from Stationary Sources. March 18, 1987.
  8. Cheney, J.L. and C.R. Fortune. Improvements in the Methodology for Measuring Hydrochloric Acid in Combustion Source Emissions. *J. Environ. Sci. Health.* A19(3): 337-350. 1984.
  9. Stern, D.A., B.M. Myatt, J.F. Lachowski, and K.T. McGregor. Speciation of Halogen and Hydrogen Halide Compounds in Gaseous Emissions. In: *Incineration and Treatment of Hazardous Waste: Proceedings of the 9th Annual Research Symposium*, Cincinnati, Ohio, May 2-4, 1983. Publication No. 600/9- 84-015. July 1984. Available from National Technical Information Service, Springfield, VA 22161 as PB84-234525.
  10. Holm, R.D. and S.A. Barksdale. Analysis of Anions in Combustion Products. In: *Ion Chromatographic Analysis of Environmental Pollutants*, E. Sawicki, J.D. Mulik, and E. Wittgenstein (eds.). Ann Arbor, Michigan, Ann Arbor Science Publishers. 1978. pp. 99-110.

## Standard Operating Procedure for the Sampling of Hydrogen Halides (Hx) and Halogens from Source Emission

### 1.0 Purpose and Applicability

This method is applicable for determining emissions of hydrogen halides (HX) and halogens from stationary sources. Same method may be applicable for those sources, which are controlled by wet scrubbers and emit acidic particulate matter.

### 1.1 Detection Limit

The in-stack detection limit is approximately  $0.05 \mu\text{g}$  / liter of stack gas; the analytical detection limit is  $0.1 \mu\text{g}$  / ml.

### 2.0 Pre sampling activity

- Rinse all sampling train glassware with hot tap water and then wash in hot soapy water.
- Rinse glassware three times with tap water, followed by three additional rinses with distilled water.
- Soak all glassware in a 10 percent (V/V) nitric acid solution for a minimum of 2 hours,
- Later rinse three times with distilled water, rinse finally with acetone, and allow to air dry cover all glassware openings where contamination can occur until the sampling train is assembled for sampling.

### 3.0 Preparation of Reagents

#### 3.1 Sampling Reagent

- Deionized, distilled water
- Sulfuric Acid ( $\text{H}_2\text{SO}_4$ ) 0.1 N
- Add 0.28 ml of concentrated  $\text{H}_2\text{SO}_4$  to 90 ml of distilled water while stirring.
- Make final volume upto 100 ml for front impinger pair.
- Sodium Hydroxide (NaOH) (0.1 N)
- Dissolve 0.40 g of solid NaOH in 90 ml of water and make final volume up to 100 ml for third and fourth impinger.
- Sodium Thiosulfate ( $\text{Na}_2\text{S}_2\text{O}_3 \cdot 5\text{H}_2\text{O}$ ) powder.

#### 3.2 Analytical Reagents

- Deionised / nano pure distilled water
- Absorbing Solution Blanks



- Stock Standard Solutions
- Field activities start with the collection of details information from the industry about products, materials, fuel and stack.

#### **4.0 Field Activities and Isokinetic Sampling**

Determine the stack pressure, temperature, leak check, calculation of Isokinetic velocity, volumetric flow rate, flow at nozzle/ selection of nozzle, adjustment of flow rate at rotameter, temperature at metering point and volume of gas sampled, pressure drop during sampling as described in the SOP of the particulate matter.

*Note:*

*For the Calculation of isokinetic velocity and collection of the sample refer Method -1 "Stack monitoring – Material and Methodology for Isokinetic Sampling" or SOP for the particulate matter determination*

#### **5.0 Preparation of the Sampling Train**

- Pour 50 ml of the acidic absorbing solution into each one of the first pair of impingers
- Pour 50 ml of the alkaline absorbing solution into each one of the second pair of impingers
- Connect the impinger in series with empty knockout impinger first if used (See Figure 1)
- Place a fresh charge of silica gel, or equivalent, in the drying tube or impinger (after the one more optional empty impinger) at the end of the impinger train.
- Adjust the probe temperature and the temperature of the filter and the stopcock temperature sufficient to prevent water condensation. Temperature should be at least 20 °C above the source temperature, but not greater than 120 °C. The temperature should be monitored to ensure that the desired temperature is maintained.

#### **6.0 Sample Collection**

- Turn on the vacuum pump and make a slight vacuum of 25 mm Hg (1 in. Hg). Set the sampling rate in gaseous train at 2 LPM & allow rest of the flow for Isokinetic sampling rate in particulate train.
- Take readings of the dry gas meter volume and temperature, rotameter, and vacuum gauge at least once every five minutes during the run.
- Sampling should be carried out for 1 hr or for the duration sufficient to collect samples to be detected above detection limit.
- During calculation of volume of air passes through the impinger & filter should be done by adding both the flow rate multiplied by sampling time.
- At the completion of sampling remove the train from the stack and cool it.



## 7.0 Sample Recovery

- Collect filter separately. No heating should be done in conditioning of filter preferably desiccation or use of conditioning room is suggested.
- Disconnect the impingers; quantitatively transfer the contents of the acid impingers and the first empty impinger, if used, to a leak-free storage bottle.
- Add the water rinses of each of these impingers and connecting glassware to the storage bottle. Quantity of rinsing should not be used more than 25ml.
- Repeat this procedure for the alkaline impingers and connecting glassware using a separate storage bottle. Quantity of rinsing water should not be used more than 25ml.
- Add 25 mg sodium thiosulfate to ensure complete reaction with the hypohalous acid to form second Cl<sup>-</sup> ion in the alkaline solution.
- Save portions of the absorbing reagents (0.1 N H<sub>2</sub>SO<sub>4</sub> and 0.1 N NaOH) equivalent to the amount used in the sampling train dilute to the approximate volume of the corresponding samples using rinse water directly from the wash bottle being used. Add the same (25mg) amount of sodium thiosulfate solution to the 0.1 N NaOH absorbing solution blank.
- Also, save a portion of the rinse water used to rinse the sampling train. Place each in a separate, pre-labeled storage bottle. The sample storage bottles should be sealed, shaken to mix, and labeled. Mark the fluid level.

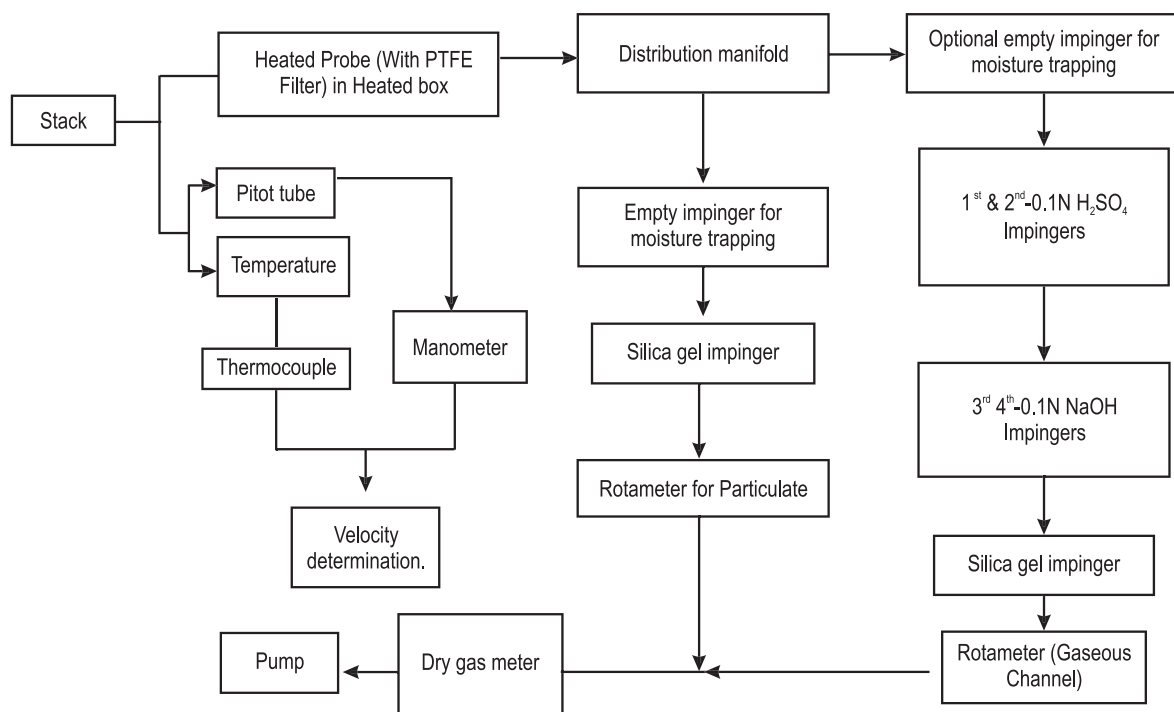


Fig - 1: Integrated Sampling train for particulate and gaseous H, and Halogens

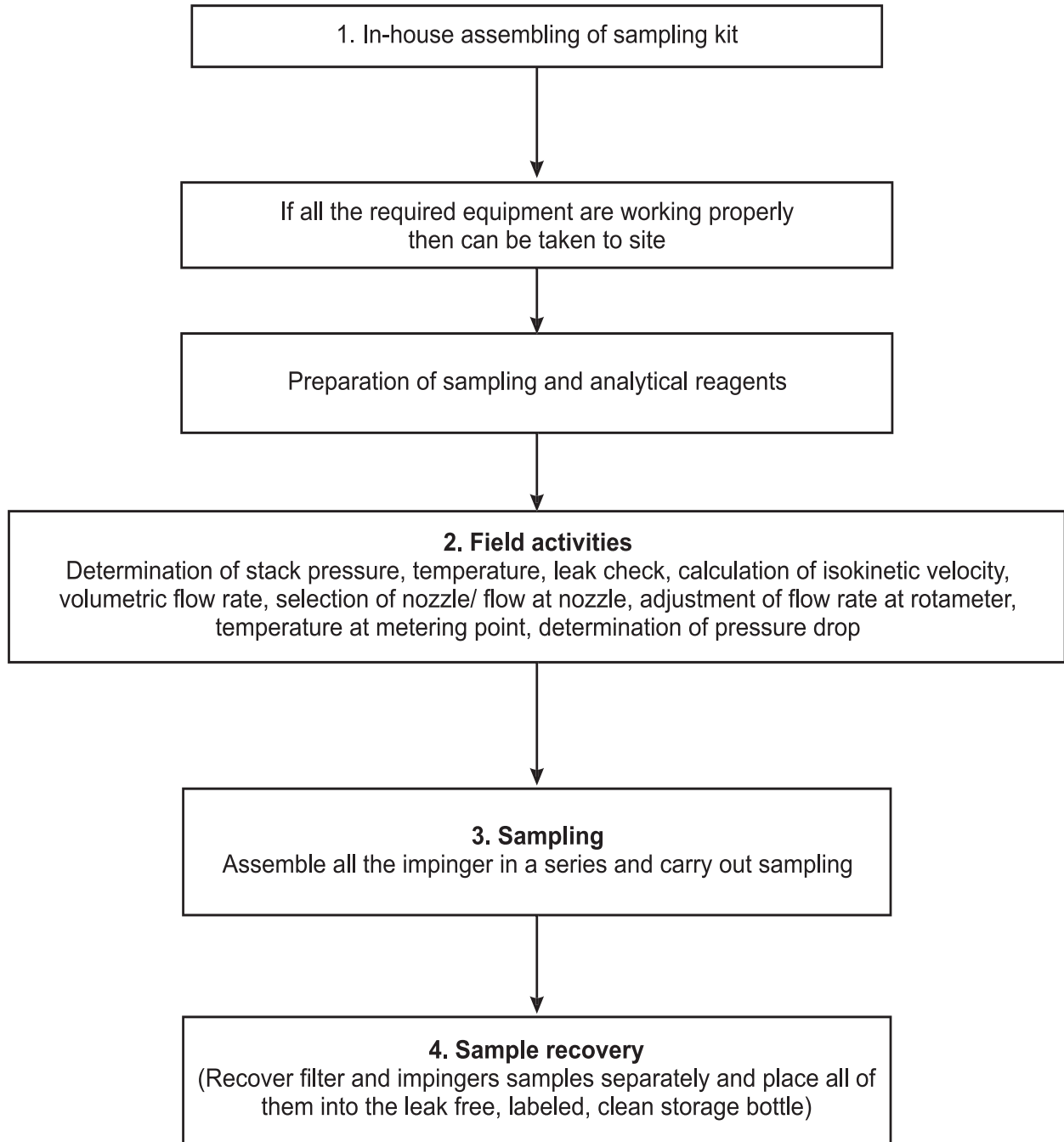


Figure 2: Sampling activity scheme

**Table - 1**  
**Field Data Sheet**

**Name & Address**

**Date & time of sampling**

**Ambient temperature °C**

**Barometric Pressure (mm mercury column)**

**Moisture in the flue gas (%) flue gas composition (CO<sub>2</sub> %, O<sub>2</sub> %, N<sub>2</sub>)**

**Filter No and weight ( Initial as well as Final)**

| Travers Point | ΔP (mm) | Ts (°K) | Ps | Us (m/s) | Qs (m <sup>3</sup> /hr) | Rs (LPM) | P <sub>m</sub>  |                 | Rm (LPM) | Time (min) | DGM (M <sup>3</sup> ) |       | V <sub>std</sub> (Nm <sup>3</sup> ) |
|---------------|---------|---------|----|----------|-------------------------|----------|-----------------|-----------------|----------|------------|-----------------------|-------|-------------------------------------|
|               |         |         |    |          |                         |          | P <sub>m0</sub> | P <sub>m1</sub> |          |            | Initial               | Final |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |

ΔP = Stack Gas Velocity Pressure, (mm water column), Ts = Stack temperature (°K)

Ps = Static pressure (mm water column), Us = Velocity of stack gas (m/s),

Qs = Volumetric Flow rate / discharge, Rs = Flow at nozzle (LPM),

Pm = Vacuum Pressure Drop (mm mercury column),

Rm = Determination of sampling rate at gas meter. (LPM),

Vstd = Determination of volume of gas sampled

**Other required information:**

- o Feed rate of hazardous waste
- o The nature, composition and quantity of the material being incinerated during monitoring
- o Installed and operating capacity of the incinerator
- o No of sampling ports
- o Internal diameter of the stack
- o Nozzle size selected for sampling
- o Pitot tube constant
- o ID fan capacity
- o Pollution control equipment installed and its status
- o House keeping

**Signature of sample collector**

**Verified by**

**Approved by**

**Occupier/  
Representative of  
the incinerator facility**

# CHAPTER - 5

## DETERMINATION OF METALS AND NON METALS EMISSIONS FROM STATIONARY SOURCES

### 1.0 PRINCIPLE

A stack sample is withdrawn isokinetically from the source, particulate emissions are collected in the probe and on a heated filter, and gaseous emissions are then collected in an aqueous acidic solution of hydrogen peroxide (analyzed for all metals including Hg) and an aqueous acidic solution of potassium permanganate (analyzed only for Hg). The recovered samples are digested, and appropriate fractions are analyzed for Hg by cold vapor atomic absorption spectroscopy (CVAAS) and for Sb, As, Ba, Be, Cd, Cr, Co, Cu, Pb, Mn, Ni, P, Se, Ag, Tl, and Zn by inductively coupled argon plasma emission spectroscopy (ICAP) or atomic absorption spectroscopy (AAS). Graphite furnace atomic absorption spectroscopy (GFAAS) is used for analysis of Sb, As, Cd, Co, Pb, Se, and Tl if these elements require greater analytical sensitivity then can be obtained by ICAP. One can choose AAS for analysis of all listed metals. Similarly, inductively coupled plasma-mass spectroscopy (ICP-MS) may be used for analysis of Sb, As, Ba, Be, Cd, Cr, Co, Cu, Pb, Mn, Ni, As, Tl and Zn.

### 2.0 APPLICABILITY

This method is applicable for determination of antimony (Sb), arsenic (As), barium (Ba), beryllium (Be), cadmium (Cd), chromium (Cr), cobalt (Co), copper (Cu), lead (Pb), manganese (Mn), mercury (Hg), nickel (Ni), phosphorus (P), selenium (Se), silver (Ag), thallium (Tl), and zinc (Zn) emissions from stationary sources. This method may be used to determine particulate emissions in addition to the metals emissions if the prescribed procedures and precautions are followed.

### 2.1 Range and sensitivity

| Metal     | Front - half:<br>Probe and Filter | Back - half:<br>Impingers 1-3 | Back - half:<br>Impingers 4-6 <sup>a</sup> | Total Train:             |
|-----------|-----------------------------------|-------------------------------|--|--------------------------|
| Antimony  | <sup>1</sup> 7.7 (0.7)            | <sup>1</sup> 3.8(0.4)         |  | <sup>1</sup> 11.5(1.1)   |
| Arsenic   | <sup>1</sup> 12.7 (0.3)           | <sup>1</sup> 6.4 (0.1)        |  | <sup>1</sup> 19.1 (0.4)  |
| Barium    | 0.5                               | 0.3                           |  | 0.8                      |
| Beryllium | <sup>1</sup> 0.07 (0.05)          | <sup>1</sup> 0.04 (0.03)      |  | <sup>1</sup> 0.11 (0.08) |
| Cadmium   | <sup>1</sup> 1.0 (0.02)           | <sup>1</sup> 0.5 (0.01)       |  | <sup>1</sup> 1.5 (0.03)  |

|            |                        |                        |                  |                         |
|------------|------------------------|------------------------|------------------|-------------------------|
| Chromium   | <sup>1</sup> 1.7 (0.2) | <sup>1</sup> 0.8 (0.1) |                  | <sup>1</sup> 2.5 (0.3)  |
| Cobalt     | <sup>1</sup> 1.7 (0.2) | <sup>1</sup> 0.8 (0.1) |                  | <sup>1</sup> 2.5 (0.3)  |
| Copper     | 1.4                    | 0.7                    |                  | 2.1                     |
| Lead       | <sup>1</sup> 10. (0.2) | <sup>1</sup> 5.0 (0.1) |                  | <sup>1</sup> 15.1 (0.3) |
| Manganese  | <sup>1</sup> 0.5 (0.2) | <sup>1</sup> 0.2 (0.1) |                  | <sup>1</sup> 0.7 (0.3)  |
| Mercury    | <sup>2</sup> 0.06      | <sup>2</sup> 0.3       | <sup>2</sup> 0.2 | <sup>2</sup> 0.56       |
| Nickel     | 3.6                    | 1.8                    |                  | 5.4                     |
| Phosphorus | 18                     | 9                      |                  | 27                      |
| Selenium   | <sup>1</sup> 18 (0.5)  | <sup>1</sup> 9. (0.3)  |                  | <sup>1</sup> 27 (0.8)   |
| Silver     | 1.7                    | 0.9 (0.7)              |                  | 2.6                     |
| Thallium   | <sup>1</sup> 9.6 (0.2) | <sup>1</sup> 4.8 (0.1) |                  | <sup>1</sup> 14.4 (0.3) |
| Zinc       | 0.5                    | 0.3                    |                  | 0.8                     |

<sup>a</sup>Mercury analysis only.

<sup>1</sup>Detection limit when analyzed by GFAAS.

<sup>2</sup>Detection limit when analysed by CVAAS, estimated for Back-half and total train.

*Note: Actual method detection limits may vary from these values, because the stack kit, QA/QC, expertise in sampling and analyses here considered as per USEPA.*

### 3.0 INTERFERENCES

Iron (Fe) can be a spectral interference during the analysis of As, Cr, and Cd by ICAP. Aluminum (Al) can be a spectral interference during the analysis of As and Pb by ICAP. Generally, these interferences can be reduced by diluting the analytical sample, but such dilution raises the in-stack detection limits. Background and overlap corrections may be used to adjust for spectral interferences.

#### 3.1 Sampling Train

It has general similarities to the particulate sampling train. A schematic of the sampling train is shown in Figure-1.

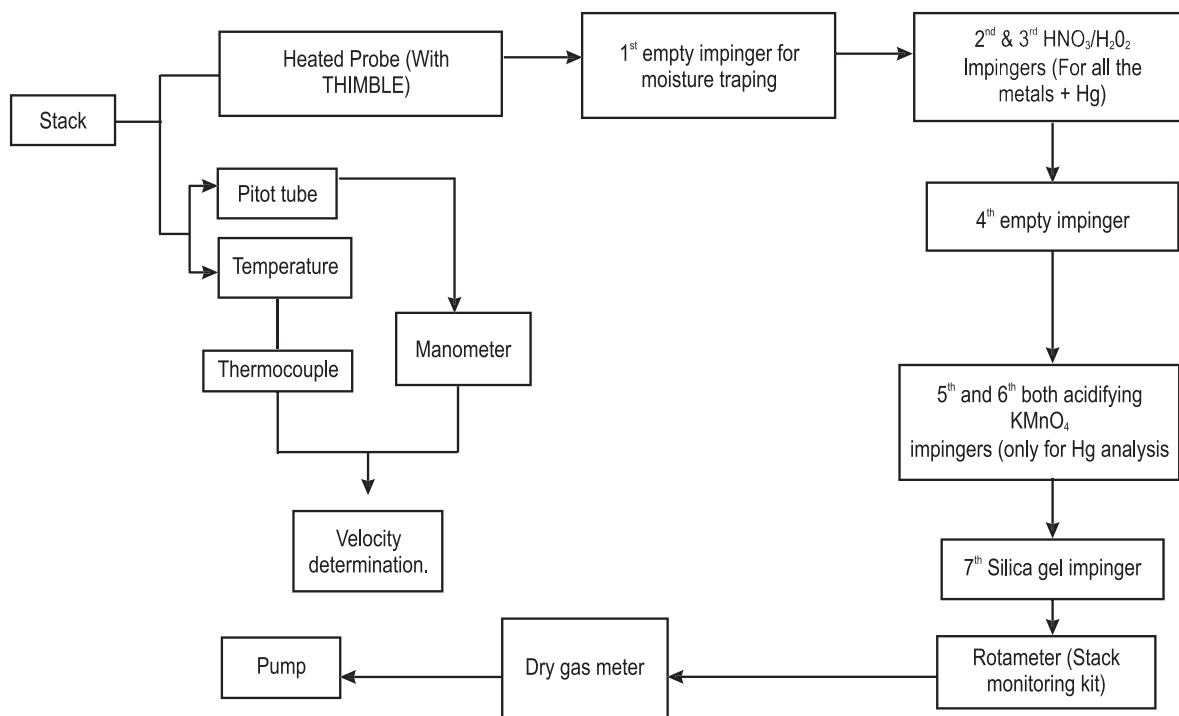


Fig - 1: Sampling train for Metals and Non Metals

### 3.1.1 Condenser

Use the following system for condensing and collecting gaseous metals and determining the moisture content of the stack gas. The condensing system shall consist of four to seven impingers connected in series with leak-free ground glass fittings or other leak-free, non-contaminating fittings. Use the first impinger as a moisture trap. The second impinger (which is the first HNO<sub>3</sub> /H<sub>2</sub>O<sub>2</sub> impinger) shall be identical to the first impinger. The third impinger (which is the second HNO<sub>3</sub> / H<sub>2</sub>O<sub>2</sub> impinger) shall be a Greenburg Smith impinger with the standard tip. The fourth (empty) impinger and the fifth and sixth (both acidified KMnO<sub>4</sub>) impingers. Place a thermometer capable of measuring temperature of 1 °C at the outlet of the last impinger. If no Hg analysis is planned, then the fourth, fifth, and sixth impingers are not required.

## 4.0 REAGENTS

### 4.1 Sampling Reagents

Table 1 : Sampling reagents

| S No. | Reagent                                | Description  |
|-------|--|--|
| 1     | Sample Filters without organic binders | The filters shall contain less than 1.3 µg/in. of each of the metals to be measured. However, if glass fiber filters become available which meet these requirements, they may be used. |

|   |  |  |
|---|--|--|
| 2 | Ultrapure Distilled Water                          | All target metals should be less than 1 ng/ml. |
| 3 | Nitric Acid (HNO <sub>3</sub> ).                   | Concentrated.                                  |
| 4 | Hydrochloric Acid (HCL).                           | Concentrated                                   |
| 5 | Hydrogen Peroxide (H <sub>2</sub> O <sub>2</sub> ) | 30 Percent (V/V).                              |
| 6 | Potassium Permanganate (KMnO <sub>4</sub> ).       |  |
| 7 | Sulfuric Acid (H <sub>2</sub> SO <sub>4</sub> ).   | Concentrated                                   |
| 8 | Silica Gel and Crushed Ice                         |  |

#### 4.2 Pretest Preparation of Sampling Reagents

**Tabel 2 : Preparation of sampling reagents**

| S. No. | Reagent  | Procedure for preparation   |
|--------|--|---|
| 1      | HNO <sub>3</sub> /H <sub>2</sub> O <sub>2</sub> Absorbing Solution, 5 Percent HNO <sub>3</sub> /10 Percent H <sub>2</sub> O <sub>2</sub> | Add carefully with stirring 50 ml of concentrated HNO <sub>3</sub> to a 1000-ml volumetric flask containing approximately 500 ml of water, and then add carefully with stirring 333 ml of 30 percent H <sub>2</sub> O <sub>2</sub> . Dilute to volume with water. Mix well. This reagent shall contain less than 2 ng/ml of each target metal.  |
| 2      | Acidic KMnO <sub>4</sub> Absorbing Solution  | Dissolve, with stirring, 40 g of KMnO <sub>4</sub> into 100 ml percent H <sub>2</sub> SO <sub>4</sub> (V/V) and add 10 percent H <sub>2</sub> SO <sub>4</sub> (V/V) with stirring to make volume of 1 liter. Prepare and store in glass bottles to prevent degradation. This reagent shall contain less than 2 ng/ml of Hg.<br><b>Precaution:</b> To prevent autocatalytic decomposition of the permanganate solution, filter the solution through whatman 541 filter paper. Also, due to the potential reaction of the potassium permanganate with the acid, there could be pressure buildup in the solution storage bottle. Therefore, these bottles shall not be fully filled and shall be vented to relieve excess pressure and prevent explosion potentials. Venting is required, but not in a manner that will allow contamination of the solution. |

|   |                       |  |
|---|-----------------------|--|
| 3 | 0.1N HNO <sub>3</sub> | Add with stirring 6.3 ml of concentrated HNO <sub>3</sub> (70 Percent) to a flask containing approximately 900 ml of water. Dilute to 1000 ml with water. Mix well. This reagent shall contain less than 2 ng/ml of each target metal. |
| 4 | 8 N HCl               | Carefully add with stirring 690 ml of concentrated HCl to a flask containing 250 ml of water. Dilute to 1000 ml with water. Mix well. This reagent shall contain less than 2 ng/ml of Hg.  |

## 5.0 PROCEDURE

### 5.1 Sampling

The complexity of this method is such that, to obtain reliable results, both testers and analysts must be trained and experienced with the test procedures, including source sampling; reagent preparation and handling; sample handling; safety equipment and procedures; analytical calculations; reporting; and the specific procedural descriptions throughout this method.

#### 5.1.1 Pretest preparation

Unless particulate emissions are to be determined, the filter need not be desiccated or weighed. First, rinse all sampling train glassware with hot tap water and then wash in hot soapy water. Next, rinse glassware three times with tap water, followed by three additional rinses with water. Then soak all glassware in a 10 percent (V/V) nitric acid solution for a minimum of 4 hours, rinse three times with water, rinse a final time with acetone, and allow to air dry. Cover all glassware openings where contamination can occur until the sampling train is assembled for sampling.

#### 5.1.2 Preliminary determinations

Perform leak check. Determine the stack pressure, temperature, calculation of Isokinetic velocity, volumetric flow rate, flow at nozzle/ selection of nozzle, adjustment of flow rate at rotameter, temperature at metering point and volume of gas sampled, pressure drop during sampling as described in the SOP of the particulate matter.

*Note:*

*Calculate isokinetic velocity and collect the sample following the SOP prescribed for particulate monitoring.*

#### 5.1.3 Preparation of sampling train:

- a. Set up the sampling train as shown in Figure-1.



- b. Use the first impinger (empty) as a moisture trap.
- c. Place 100 ml of the  $\text{HNO}_3/\text{H}_2\text{O}_2$  solution in each of the second and third impingers as shown in Figure -1.
- d. Keep another Empty impinger in 4th position.
- e. Place 100 ml of the acidic  $\text{KMnO}_4$  absorbing solution in each 5th and 6th impingers as shown in Figure 1,
- f. Transfer approximately 200 to 300 g of pre-weighed silica gel from its container to the last impinger.
- g. If Hg analysis will not be performed, the fourth, fifth, and sixth impingers as shown in Figure -1 are not required.
- h. To insure leak-free sampling train connections and to prevent possible sample contamination problems, use Teflon tape or other non-contaminating material instead of silicone grease.

**Precaution:**

- Exercise extreme care to prevent contamination within the train.
- Prevent the acidic  $\text{KMnO}_4$  from contacting any glassware that contains sample material to be analyzed for Mn. Prevent acidic  $\text{H}_2\text{O}_2$  from mixing with the acidic  $\text{KMnO}_4$ .
- Leak Check Procedures. Initial and final reading in Hg guage should be noted. If the pressure drop during sampling is not quantifiable then the whole process shall be repeated after ensuring there is no leak in sampling train

**5.2 Sample Recovery**

Begin cleanup procedures as soon as the probe is removed from the stack at the end of a sampling period. The probe should be allowed to cool prior to sample recovery. When it can be safely handled, wipe off all external particulate matter near the tip of the probe nozzle and place a rinsed, non-contaminating cap over the probe nozzle to prevent losing or gaining particulate matter. Do not cap the probe tip tightly while the sampling train is cooling; a vacuum can form in the filter holder with the undesired result of drawing liquid from the impingers onto the filter. Before moving the sampling train to the cleanup site, remove the probe from the sampling train and cap the open outlet. Be careful not to lose any condensate that might be present. Cap the filter inlet where the probe was fastened. Remove the umbilical cord from the last impinger and cap the impinger. Cap the filter holder Outlet and impinger inlet. Use non contaminating caps, whether ground-glass stoppers, plastic caps, serum caps, or Teflon tape to close these openings.

Transfer the probe and filter-impinger assembly to a cleanup area that is clean and protected from the wind and other potential causes of contamination or loss of sample. Inspect the train before and during disassembly and note any abnormal conditions. Take special precautions to assure that all the items necessary for recovery do not contaminate the samples.

### **Container No.1 (Sample Filter)**

Carefully remove the filter from the filter holder and place it in its labeled petri dish container. To handle the filter, use either acid washed polypropylene or Teflon coated tweezers or clean, disposable surgical gloves rinsed with water and dried. If it is necessary to fold the filter, make certain the particulate cake is inside the fold. Carefully transfer the filter and any particulate matter or filter fibers that adhere to the filter holder gasket to the Petri dish by using a dry (acid cleaned) nylon bristle brush. Do not use any metal- containing materials when recovering this train. Seal the labeled Petri dish. See the Figure – 2.

### **Container No. 2 (Probe Rinse)**

Keep the probe assembly clean and free from contamination during the probe rinse. Rinse the probe nozzle and fitting, probe liner, and front-half of the filter holder thoroughly with a total of 100 ml of 0.1 N HNO<sub>3</sub> and place the wash into a sample storage container.

*Note: The use of exactly 100 ml is necessary for the subsequent blank correction procedures. Record the volume of the rinses Mark the height of the fluid level on the outside of the Storage container and use this mark to determine if leakage occurs during transport. Seal the container, and clearly label the contents. Finally, rinse the nozzle, probe liner, and front-half of the filter holder with water followed by acetone, and discard these rinses. (See figure – 2).*

### **Container No. 3 (Impingers 1 through 3**

Moisture Knockout Impinger when used, HNO<sub>3</sub>/H<sub>2</sub>O<sub>2</sub> Impingers Contents and Rinses). Due to the potentially large quantity of liquid involved, the tester may place the impinger solutions from impingers 1 through 3 in more than one container, if necessary. Measure the liquid in the first three impingers to within 0.5 ml using a graduated cylinder. Record the volume. This information is required to calculate the moisture content of the sampled flue gas. Clean each of the first three impingers, the filter support, the back half of the filter housing, and connecting glassware by thoroughly rinsing with 100 ml of 0.1 N HNO<sub>3</sub>

*Note: The use of exactly 100 ml of 0.1 N HNO<sub>3</sub> rinse is necessary for the subsequent blank correction procedures. Combine the rinses and impinger solutions, measure and record the final total volume. Mark the height of the fluid level, seal the container, and clearly label the contents. (See figure 2.1)*

Container Nos.4A (0.1 N HNO<sub>3</sub>), 4B (KMnO<sub>4</sub>/H<sub>2</sub>SO<sub>4</sub> absorbing solution), and 4C (8 N HCl rinse and dilution).

When sampling for Hg, pour the liquid from impinger No. 4 into a graduated cylinder and measure the volume to within 0.5 ml. This information is required to calculate the moisture content of the sampled flue gas. Place the liquid in Container No. 4A. Rinse the impinger with exactly 100 ml of 0.1 N HNO<sub>3</sub> and place this rinse in Container No. 4A.

Pour all the liquid from the two permanganate impingers into a graduated cylinder and measure the volume to within 0.5 ml. This information is required to calculate the moisture content of the sampled flue gas. Place this acidic KMnO<sub>4</sub> solution into Container No. 4B. Using a total of exactly 100 ml of fresh acidified KMnO<sub>4</sub> solution for all rinses (approximately 33 ml per rinse), Similarly, using 100 ml total of water, rinse the permanganate impingers and connecting glass a minimum of three times, and pour the rinses into Container 4B, carefully assuring transfer of any loose precipitated material. Mark the height of the fluid level, and clearly label the contents.

*NOTE: Due to the potential reaction of KMnO<sub>4</sub> with acid, pressure buildup can occur in the sample storage bottles. Do not fill these bottles completely and take precautions to relieve excess pressure.*

If deposits remain on the impinger surfaces, wash them with 25 ml of 8 N HCl, and place the wash in a separate sample Container No. 4C containing 200 ml of water. First, place 200 ml of water in the container. Then wash the impinger walls and stem with the HCl by turning the impinger on its side and rotating it so that the HCl contacts all inside surfaces. Use a total of only 25 ml of 8 N HCl for rinsing both permanganate impingers combined. Rinse the first impinger, then pour the actual rinse used for the first impinger into the second impinger for its rinse. Finally, pour the 25 ml of 8 N HCl rinse carefully into the container. Mark the height of the fluid level on the outside of the container to determine if leakage occurs during transport. See figure 2.2

### **Container No. 5 (Silica Gel)**

Note the color of the indicating silica gel to determine whether it has been completely spent and make a notation of its condition. Transfer the silica gel from its impinger to its original container and seal it. The small amount of particles that might adhere to the impinger wall need not be removed. Do not use water or other liquids to transfer the silica gel since weight gained in the silica gel impinger is used for moisture calculations. Alternatively, if a balance is available in the field, record the weight of the spent silica gel (or silica gel plus impinger) to the nearest 0.5 g.

- Container No. 6A (0.1 N HNO<sub>3</sub> Blank).
- Container No. 6B (Water Blank).
- Container No. 7 (5 Percent HNO<sub>3</sub> /10 Percent H<sub>2</sub>O<sub>2</sub> Blank).
- Container No. 8 (Acidified KMnO<sub>4</sub> Blank).

- Container No. 9 (8 N HCl Blank).
- Container No. 10 (Sample Filter Blank)

### 5.3 Sample Preparation

Note the level of the liquid in each of the containers and determine if any sample was lost during shipment. A diagram illustrating sample preparation and analysis procedures for each of the sample train components is shown in Figure –3 and Figure - 3.1

#### Container No. 1 (Sample Filter)

If particulate emissions are being determined, first desiccate the filter and filter catch without added heat (do not heat the filters to speed the drying) and weigh to a constant weight as described in the term “constant weight” means a difference of no more than 0.5 mg or 1 percent of total weight less tare weight, whichever is greater, between two consecutive weighing, with no less than 6 hours of desiccation time between two weighing.

#### Option I – Microwave digestion

Make pieces of filter papers/thimbles (Do not use metallic scissor). Place the pieces in the analyst’s choice of either individual microwave pressure relief vessels or ParrR Bombs. Add 6 ml of concentrated  $\text{HNO}_3$  and 4 ml of concentrated HF to each vessel. For microwave heating, microwave the samples for approximately 12 to 15 minutes total heating time as follows: heat for 2 to 3 minutes, then turn off the microwave for 2 to 3 minutes, then heat for 2 to 3 minutes, etc., continue this alternation until the 12 to 15 minutes total heating time are completed (this procedure should comprise approximately 24 to 30 minutes at 600 watts). Microwave heating times are approximate and are dependent upon the number of samples being digested simultaneously. Sufficient heating is evidenced by sorbent reflux within the vessel. Then cool the samples to room temperature.

#### Option II – Hot Plate Digestion

Place the pieces of thimbles in acid cleaned beaker add about 50 ml water, add 6 ml of concentrated  $\text{HNO}_3$  and 4 ml of concentrated HF to it. Place it on hot plate under fume extraction hood. Set the Temperature at 70 °C. Continue to digest for 12 hrs.

#### Container No. 2 (Probe Rinse)

Verify that the pH of this sample is 2 or lower. If it is not, acidify the sample by careful addition with stirring of concentrated  $\text{HNO}_3$  to pH 2. Use water to rinse the sample into a beaker, and cover the beaker with a ribbed watch glass. Reduce the sample volume to approximately 20 ml by heating on a hot plate at a temperature below boiling. Add 6 ml of concentrated  $\text{HNO}_3$  and 4 ml of concentrated HF to it. Place it on hot plate under fume extraction hood. Set the Temperature at 70 °C Continue the digestion for 12 hrs. If the

sampling train includes an optional glass cyclone in front of the filter, prepare and digest the cyclone catch by the same way. Then combine the resultant sample directly with the acid digested portions of the filter prepared previously, acid rinse concentrate and cyclone catch concentrate (If done). Filter the combined sample using Whatman 41 filter paper. Dilute to 300 ml (or the appropriate volume for the expected metals concentration) with water. This diluted sample is "Analytical Fraction 1". Measure and record the volume of Analytical Fraction 1 to within 0.1 ml. Quantitatively remove a 50-ml aliquot and label as "Analytical Fraction 1B". Label the remaining 250-ml portion as "Analytical Fraction 1A". Analytical Fraction 1A is used for ICAP or AAS analysis for all desired metals except Hg. Analytical Fraction 1B is used for the determination of front-half Hg. This fraction should be treated with acid and  $\text{KMnO}_4$  at  $90^\circ\text{C}$  for 2 hours. Excess  $\text{KMnO}_4$  should be removed by using Hydroxylamine Hydrochloride before analysis of Hg.

### **Container No.3 (Impingers 1-3)**

Measure and record the total volume of this sample to within 0.5 ml, if the leakage found significant make up with fresh distilled water. Remove a 75- to 100-ml aliquot for Hg analysis and label the aliquot "Analytical Fraction 3B". Label the remaining portion as "Sample Fraction 3A". Verify that the pH of Sample Fraction 3A is 2 or lower. If necessary, use concentrated  $\text{HNO}_3$  by careful addition and stirring to lower the pH upto 2. Use water to rinse Sample Fraction 3A into a beaker and then cover the beaker with a ribbed watch glass. Reduce Sample to approximately 20 ml by heating on a hot plate at a temperature just below boiling. Add 30 ml of 50 percent  $\text{HNO}_3$  and heat for 30 minutes on a hot plate to just below boiling. Add 10 ml of 3 percent  $\text{H}_2\text{O}_2$  and heat for 10 more minutes. Add 50 ml of hot water, and heat the sample for an additional 20 minutes. Cool, filter the sample, and dilute to 150 ml (or the appropriate volume for the expected metals concentrations) with water. Analytical Fraction 3A is analyzed for all metals except Hg. Analytical fraction 3B will be digested separately with HCl and  $\text{KMnO}_4$  at  $90^\circ\text{C}$  for two hours. Excess Permanganate should be removed by Hydroxylamine Hydrochloride before analysis in Cold Vapour AAS.

### **Container No. 4A (Empty impnger washing liquid with 0.1 N $\text{HNO}_3$ ), 4B ( $\text{KMnO}_4$ / $\text{H}_2\text{SO}_4$ absorbing solution of impinger 5 and 6), and 4C (8 N HCl rinse of impinger 5 and 6 for scaling of $\text{MnO}_2$ ).**

Keep the samples in Containers Nos. 4A, 4B, and 4C separate from each other. Measure and record the volume of 4A to within 0.5 ml. Concentrate the sample upto 20 ml on hot plate at below boiling temperature. Keep it separate. To remove any brown  $\text{MnO}_2$  precipitate from the contents of Container No. 4B, filter its contents through Whatman 40 filter paper into a 500 ml volumetric flask, make up the volume with distilled water. This fraction is analytical fraction 4B. Save the filter for digestion of the brown  $\text{MnO}_2$  precipitate. Place the saved filter into an appropriately sized vented container, which will allow release of any gases including chlorine formed when the filter is digested in a laboratory hood. Add 25 ml of 8 N

HCl to the filter and allow to digest for a minimum of 24 hours at room temperature. Filter the contents of Container No. 4C through a Whatman 40 filter into a 500-ml volumetric flask. Then filter the result of the digestion of the brown MnO<sub>2</sub> from Container No. 4B through a Whatman 40 filter into the same 500-ml volumetric flask, and dilute and mix well to volume with water. Discard the Whatman 40 filter. Mark this combined 500-ml dilute HCl solution as Analytical fraction 4C. So three samples will be generated in this section for Hg analysis. All these fractions shall be digested and concentrated to desired volume with HCl and KMnO<sub>4</sub> at 90 °C for two hours. Excess Permanganate should be removed by Hydrxylamine Hydrochloride before analysis in Cold Vapour AAS.

### Container No. 6 (Silica Gel)

Weigh the spent silica gel (or silica gel plus impinger) to the nearest 0.5 g using a balance.

## 5.4 Sample Analysis

For each sampling train sample run, seven individual analytical samples are generated ; two (Analytical fraction 1A and 3A) for all desired metals except Hg, and five for Hg (Analytical fraction 1B, 3B, 4A, 4B and 4C). A schematic identifying each sample container and the prescribed analytical preparation and analysis scheme is shown in Figure 3 and Figure 3.1. Blanks for all reagents used should be processed with samples in parallel.

## 6.0 CALCULATIONS

For Molecular weight determination, Stack gas velocity, Isokinetic Flow rate, Moisture content and parameters required for particulate emission calculation follow the formulae mentioned in method prescribed for particulate matter determination.

Dry Gas Volume. Using the data from this test, calculate V , the dry gas sample volume at standard conditions m(std) as outline Correct the sample volume measured by the dry gas meter to standard conditions (25 °C, 760 mm Hg or 68 °F, 29.92 inch Hg) by using following Equation. Where, Y is DGM Calibration Factor.

$$V_{mstd} = V_m \cdot Y \left[ \frac{T_{std}}{T_m} \right] \left[ \frac{P_{bar}}{P_{std}} \right] = K_1 \cdot Y \cdot V_m \left[ \frac{P_{bar}}{P_m} \right]$$

Where:

K<sub>1</sub> = 0.3858 °K/mm Hg for metric units,  
= 17.64 °C/in. Hg for English units

P<sub>bar</sub> = Barometric pressure at the exit orifice of the DGM, mm Hg (in. Hg).

P<sub>std</sub> = Standard absolute pressure, 760 mm Hg (29.92 in.Hg).

T<sub>m</sub> = Average DGM absolute temperature, °K (°C).



$T_{std}$  = Standard absolute temperature, 293 °K

$Y$  = Dry gas meter calibration factor

$V_{m(std)}$  = Dry gas volume measured by the dry gas meter, corrected to standard conditions,  $Nm^3$

$V_m$  = {Sampling rate in gas channel (LPM) X duration (Minutes)} / 1000  $m^3$ .

Calculate all the seven fraction (2 for other metals and 5 for mercury) in mass of individual elements following the formula

### **Metals (Except Hg) in Source Sample.**

$M_x$  =  $C_x$  (ppm) \*  $D$  \*  $V_{ds}$

Where:

$M_x$  = Total mass of each metal in  $\mu g$ .

$C_x$  = Concentration of metal in respective fraction as read from the standard curve in  $\mu g/ml$  (ppm) after respective blank subtraction

$D$  = dilution Factor

$V_{ds}$  = Total volume of digested sample solution in Analytical fraction ml.

$M_x$  values calculated for fraction 1A and 3A should be added individually to represent to total mass for each metals except Hg. The concentration emitted from stack would be calculated as below.

$\{M_x(1A) + M_x(3A)\} * 10^{-3} / V_{m(std)}$   $mg/NM^3$

### **Similarly for Hg**

$\{M_x(1B) + M_x(3B) + M_x(4A) + M_x(4C)\} * 10^{-3} / V_{m(std)}$   $mg/NM^3$

**Note: Report concentration as corrected at 11%  $O_2$**

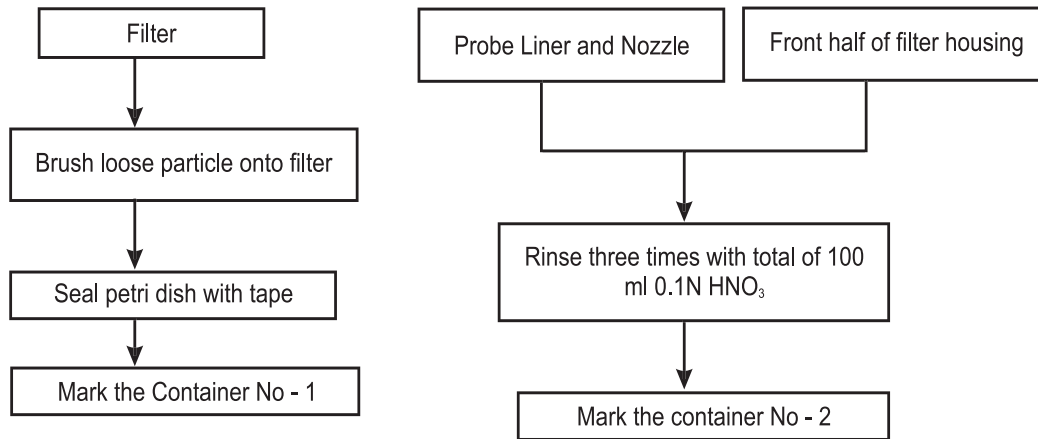


Figure -2: Sample Recovery Scheme for Sample filter, Probe rinse, Front half the filter housing

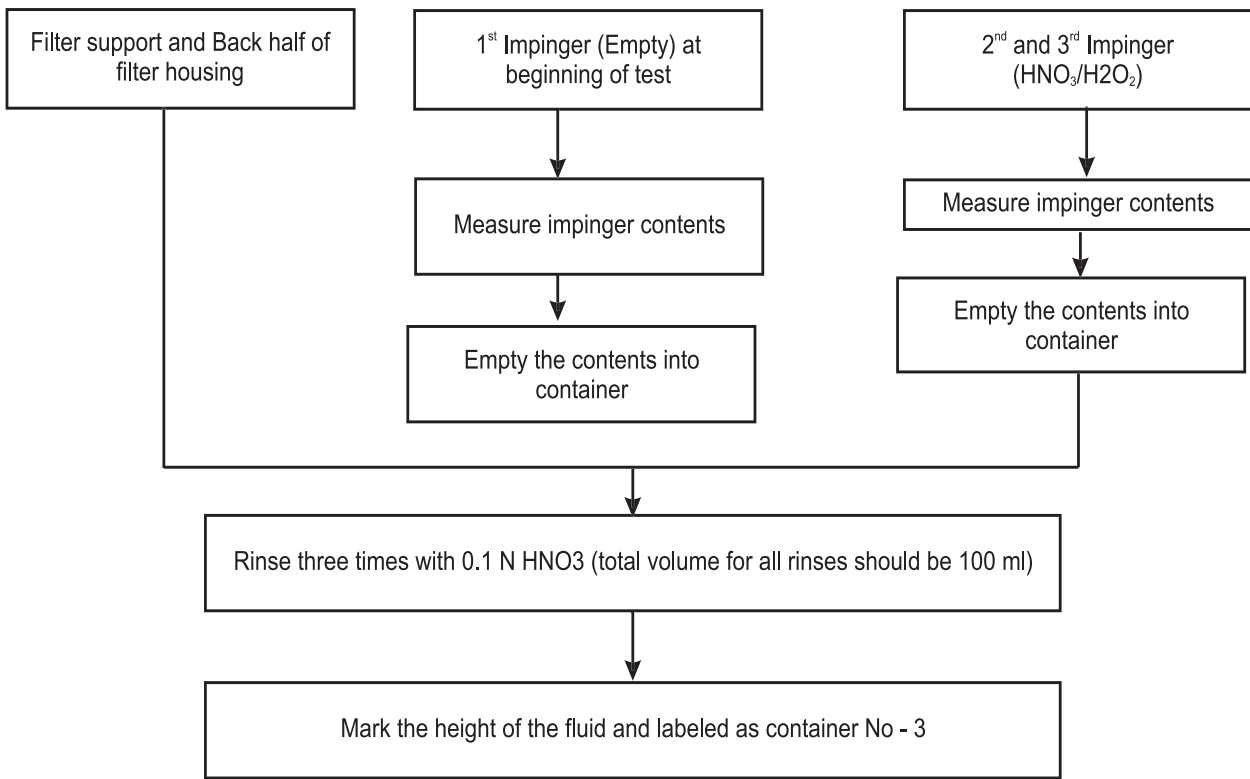
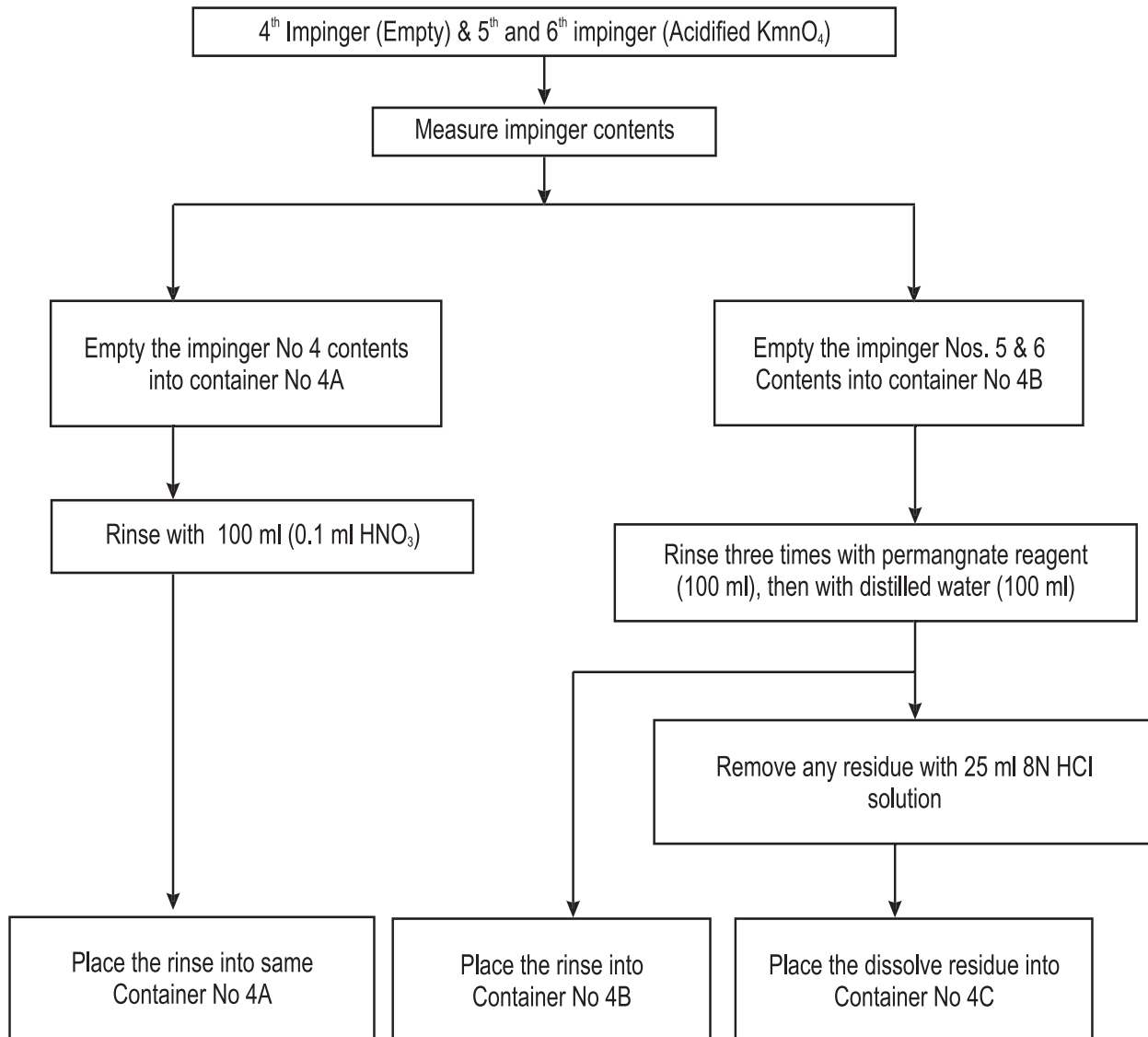
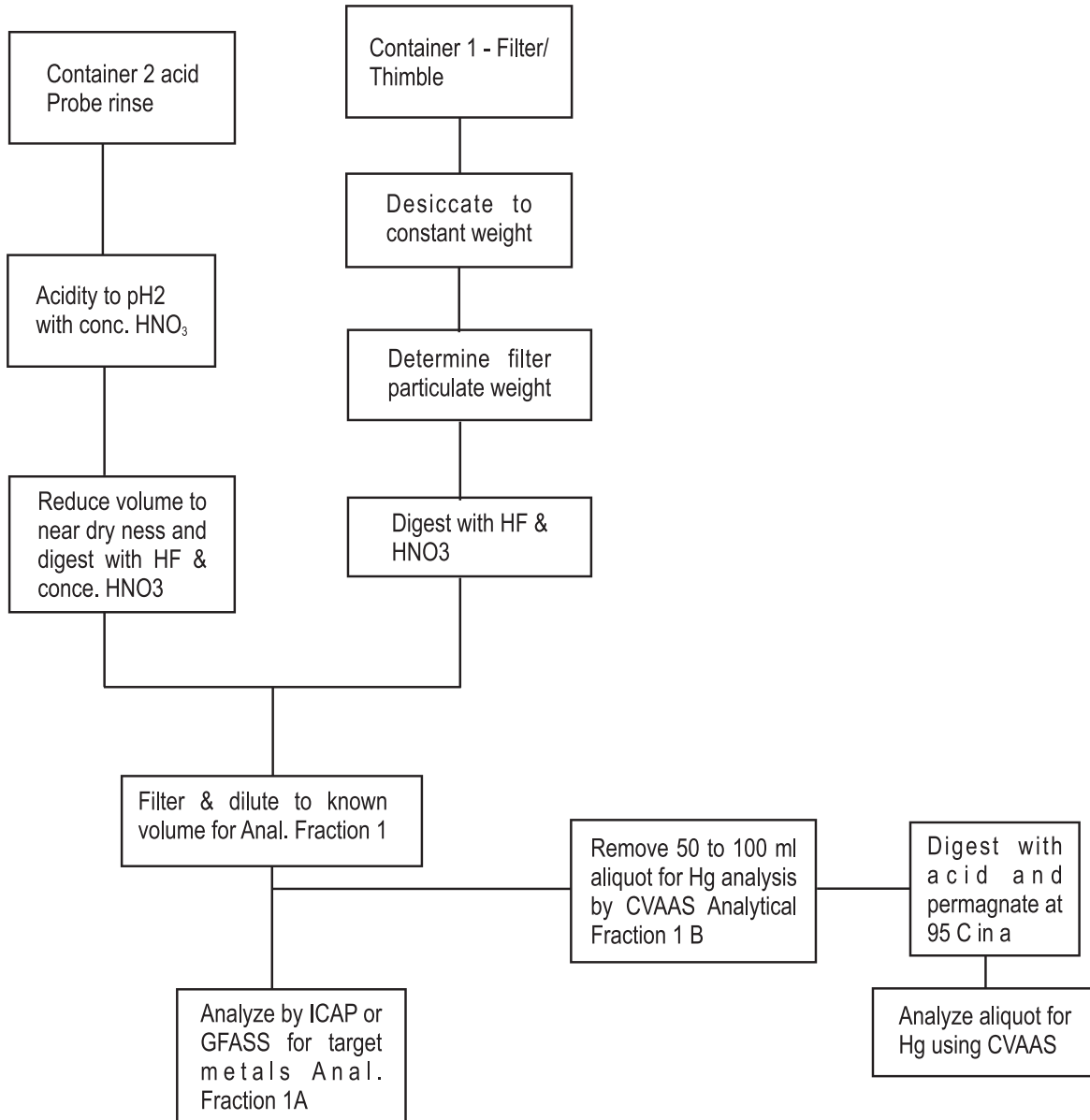


Figure -2.1: Sample Recovery Scheme for Filter support and Back half of filter housing, 1<sup>st</sup> (Empty), 2<sup>nd</sup>, 3<sup>rd</sup> Impinger (HNO<sub>3</sub>/H<sub>2</sub>O<sub>2</sub>)

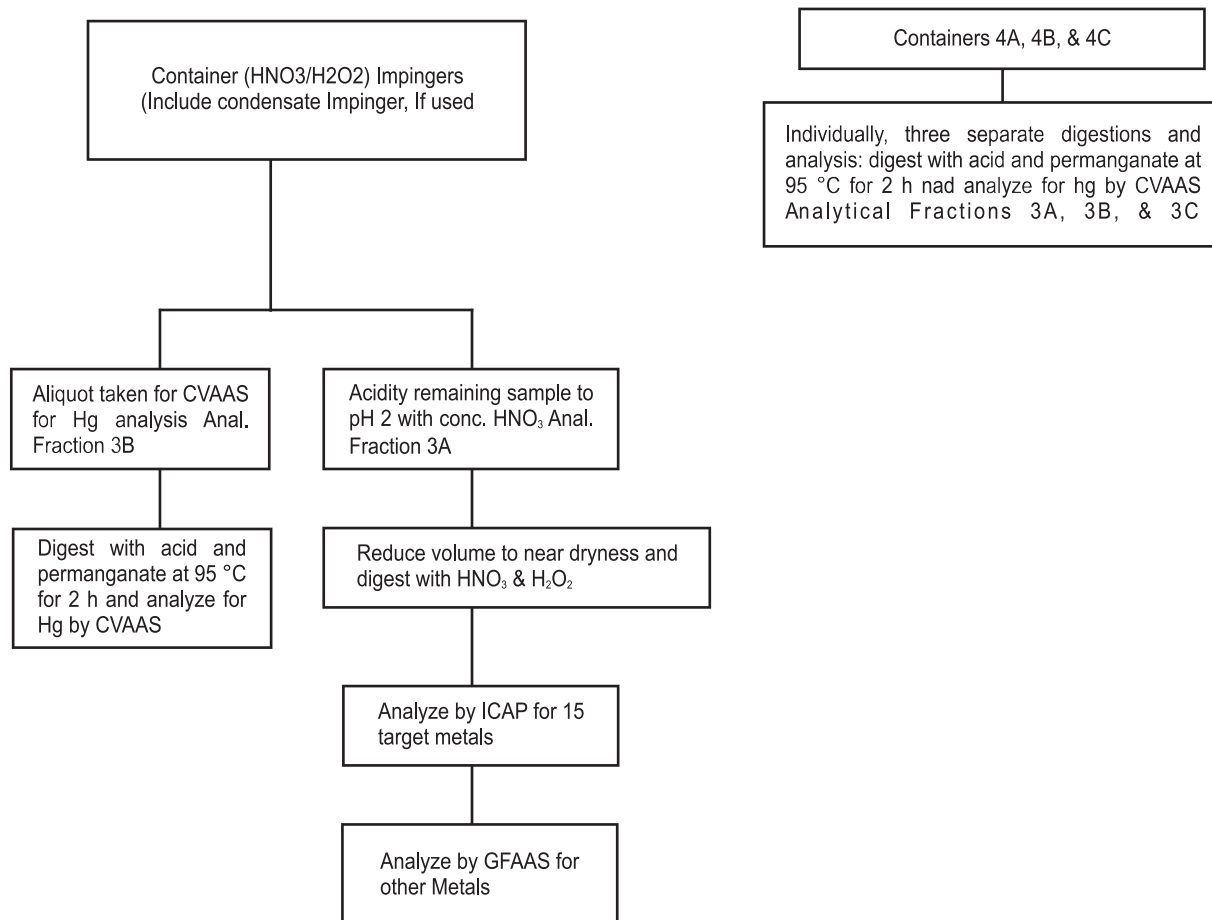




**Figure-2.2: Sample Recovery Scheme 4<sup>th</sup> Impinger (Empty) & 5<sup>th</sup> and 6<sup>th</sup> Impinger (Acidified KmnO<sub>4</sub>)**



**Figure - 3: Sample Preparation and Analysis Scheme.**



**Figure - 3.1: Sample Preparation and Analysis Scheme.**

## 7.0 REFERENCES

1. Method 303F in Standard Methods for the Examination of Water Wastewater, 15th Edition, 1980. Available from the American Public Health Association, 1015 18th Street N.W., Washington, D.C. 20036.
2. EPA Methods 6010, 6020, 7000, 7041, 7060, 7131, 7421, 7470, 7740, and 7841, Test Methods for Evaluating Solid Waste: Physical/Chemical Methods. SW-846, Third Edition, November 1986, with updates I, II, IIA and IIB. Office of Solid Waste and Emergency Response, U. S. Environmental Protection Agency, Washington, D.C. 20460.
3. EPA Method 200.7, Code of Federal Regulations, Title 40, Part 136, Appendix C. July 1, 1987.
4. EPA Methods 1 through 5, Code of Federal Regulations, Title 40, Part 60, Appendix A July 1, 1991.
5. EPA Method 101A, Code of Federal Regulations, Title 40, Part 61, Appendix B, July 1, 1991.

# CHAPTER - 6

## PART I

### STANDARD OPERATING PROCEDURE (SOP) FOR SAMPLING OF METALS AND NON METALS

&

## PART II

### STANDARD OPERATING PROCEDURE (SOP) OF SAMPLE PREPARATION FOR ANALYSIS OF METALS AND NON METALS

#### ***Disclaimer:***

*These Standard Operating Procedures (SOPs) are only guidelines for sampling and analysis of metals and non metals in incinerator stack emissions. Concerned Institutes/ Organizations/ laboratories may modify the analytical part according to their need; infrastructure and men power training involved maintaining the QA/QC protocol as required by the method.*

## Part-I

### STANDARD OPERATING PROCEDURE FOR SAMPLING OF METALS AND NON METALS

#### 1.0 Purpose and Applicability

This method is applicable for determination of antimony (Sb), arsenic (As), barium (Ba), beryllium (Be), cadmium (Cd), chromium (Cr), cobalt (Co), copper (Cu), lead (Pb), manganese (Mn), mercury (Hg), nickel (Ni), phosphorus (P), selenium (Se), silver (Ag), thallium (Tl), and zinc (Zn) emissions from stationary sources. This method may be used to determine particulate emissions in addition to the metals emissions if the prescribed procedures and precautions are followed.

#### 1.1 Range and sensitivity

| Metal     | Front - half:<br>Probe and Filter | Back - half:<br>Impingers 1-3 | Back - half:<br>Impingers 4-6 <sup>a</sup> | Total Train:             |
|-----------|-----------------------------------|-------------------------------|--|--------------------------|
| Antimony  | <sup>1</sup> 7.7 (0.7)            | <sup>1</sup> 3.8(0.4)         |  | <sup>1</sup> 11.5(1.1)   |
| Arsenic   | <sup>1</sup> 12.7 (0.3)           | <sup>1</sup> 6.4 (0.1)        |  | <sup>1</sup> 19.1 (0.4)  |
| Barium    | 0.5                               | 0.3                           |  | 0.8                      |
| Beryllium | <sup>1</sup> 0.07 (0.05)          | <sup>1</sup> 0.04 (0.03)      |  | <sup>1</sup> 0.11 (0.08) |
| Cadmium   | <sup>1</sup> 1.0 (0.02)           | <sup>1</sup> 0.5 (0.01)       |  | <sup>1</sup> 1.5 (0.03)  |
| Chromium  | <sup>1</sup> 1.7 (0.2)            | <sup>1</sup> 0.8 (0.1)        |  | <sup>1</sup> 2.5 (0.3)   |
| Cobalt    | <sup>1</sup> 1.7 (0.2)            | <sup>1</sup> 0.8 (0.1)        |  | <sup>1</sup> 2.5 (0.3)   |
| Copper    | 1.4                               | 0.7                           |  | 2.1                      |
| Lead      | <sup>1</sup> 10.1 (0.2)           | <sup>1</sup> 5.0 (0.1)        |  | <sup>1</sup> 15.1 (0.3)  |
| Manganese | <sup>1</sup> 0.5 (0.2)            | <sup>1</sup> 0.2 (0.1)        |  | <sup>1</sup> 0.7 (0.3)   |
| Mercury   | <sup>2</sup> 0.06                 | <sup>2</sup> 0.3              | <sup>2</sup> 0.2                           | <sup>2</sup> 0.56        |

|            |                        |                        |  |                         |
|------------|------------------------|------------------------|--|-------------------------|
| Nickel     | 3.6                    | 1.8                    |  | 5.4                     |
| Phosphorus | 18                     | 9                      |  | 27                      |
| Selenium   | <sup>1</sup> 18 (0.5)  | <sup>1</sup> 9. (0.3)  |  | <sup>1</sup> 27 (0.8)   |
| Silver     | 1.7                    | 0.9 (0.7)              |  | 2.6                     |
| Thallium   | <sup>1</sup> 9.6 (0.2) | <sup>1</sup> 4.8 (0.1) |  | <sup>1</sup> 14.4 (0.3) |
| Zinc       | 0.5                    | 0.3                    |  | 0.8                     |

<sup>a</sup>Mercury analysis only.

<sup>1</sup>Detection limit when analyzed by GFASS.

<sup>2</sup>Detection limit when analysed by CVAAS, estimated for Back-half and total train.

*Note: Actual method detection limits may vary from these values, because the stack kit, QA/QC, expertise in sampling and analyses here considered as per USEPA.*

## 2.0 Pre sampling activity

Rinse all sampling train glassware with hot tap water and then wash in hot soapy water. Rinse glassware three times with tap water, followed by three additional rinses with distilled water.

Soak all glassware in a 10 percent (V/V) nitric acid solution for a minimum of 4 hours, later rinse three times with distilled water, rinse finally with acetone, and allow to air dry. Cover all glassware openings where contamination can occur until the sampling train is assembled for sampling.

## 3.0 Preparation of reagent

### 3.1 Sampling Reagents

- Sample Filters without any organic binders
- Quartz or GF filters shall contain less than 1.3 µg / inch<sup>2</sup> of each of the metals to be measured.
- Ultrapure distilled water.
- Concentrated Nitric Acid (HNO<sub>3</sub>)
- Concentrated Hydrochloric Acid (HCl)

- Hydrogen Peroxide (H<sub>2</sub>O<sub>2</sub>) 30 Percent (V/V)
- Potassium Permanganate (KMnO<sub>4</sub>)
- Sulfuric Acid (H<sub>2</sub>SO<sub>4</sub>)
- Silica Gel

### 3.2 Preparation of sampling reagents

HNO<sub>3</sub> /H<sub>2</sub>O<sub>2</sub> Absorbing Solution, 5 Percent HNO<sub>3</sub> /10 Percent H<sub>2</sub>O<sub>2</sub>

Add 50 ml of concentrated HNO<sub>3</sub> to a 1000-ml volumetric flask containing approximately 500 ml of water add carefully with stirring 333 ml of 30 percent H<sub>2</sub>O<sub>2</sub>,

Make up the volume with distilled water.

Acidic KMnO<sub>4</sub> Absorbing Solution (4 % KMnO<sub>4</sub> (W/V), in 10 Percent H<sub>2</sub>SO<sub>4</sub> (V/V).

Mix carefully, with stirring, 100 ml of concentrated H<sub>2</sub>SO<sub>4</sub> into approximately 800 ml of water, and add water with stirring to make a volume of 1 liter: this solution is 10 % H<sub>2</sub>SO<sub>4</sub> (V/V). Dissolve 40 g of KMnO<sub>4</sub> into 10 percent H<sub>2</sub>SO<sub>4</sub> (V/V) and add 10 % H<sub>2</sub>SO<sub>4</sub> (V/V) with stirring to make a volume of 1 liter. Prepare and store in glass bottles to prevent degradation.

#### Note:

To prevent autocatalytic decomposition of the permanganate solution, filter the solution through Whatman 41 filter paper. Also, due to the potential reaction of the potassium permanganate with the acid, there could be pressure buildup in the solution storage bottle. Therefore, these bottles shall not be fully filled and shall be vented to relieve excess pressure and prevent explosion potentials. Venting is required, but not in a manner that will allow contamination of the solution.

#### 0.1N HNO<sub>3</sub>

Add 6.3 ml of concentrated HNO<sub>3</sub> (70 percent) to a flask containing approximately 900 ml of distilled water. Dilute to 1000 ml with distilled water.

#### 8 N HCl

Add stirring 690 ml of concentrated HCl to a flask containing 250 ml of water. Dilute to 1000 ml with water.

*Note: All the reagent shall satisfy at less than 2 ng/ml of each target metals.*

### 4.0 Preparation of sampling train

- Assemble the sampling train as shown in the Figure – 1.

- Select First impinger as a moisture trap.
- Put 100 ml of the  $\text{HNO}_3$  / $\text{H}_2\text{O}_2$  solution in the second and the third impinger.
- Keep fourth impinger empty.
- Place 100 ml of the acidic  $\text{KMnO}_4$  absorbing solution in each 5th and 6th impingers
- Take 200 to 300 g of pre-weighed silica gel in the last impinger.

If Hg analysis will not be performed, the fourth, fifth, and sixth impingers as shown in Figure -1 are not required.

**Precaution:**

- Prevent the acidic  $\text{KMnO}_4$  from contacting any glassware that contains sample material to be analyzed for Mn.
- Prevent acidic  $\text{H}_2\text{O}_2$  from mixing with the acidic  $\text{KMnO}_4$ .
- Uses of amber glass impinger are recommended for acidic  $\text{KMnO}_4$  Solution.

**5.0 Field activity**

Perform leak check. Determine the stack pressure, temperature, calculation of Isokinetic velocity, volumetric flow rate, flow at nozzle/ selection of nozzle, adjustment of flow rate at rotameter, temperature at metering point and volume of gas sampled, pressure drop during sampling as described in the SOP of the particulate matter.

*Note:*

*Calculate isokinetic velocity and collect the sample following the SOP prescribed for Particulate monitoring.*

**6.0 Sample Recovery**

Cool the probe, Transfer the probe and filter assembly to a clean area, cap all the open outlet with the non-contaminated glass stoppers or plastic cap.

Take special precautions to assure that all the items necessary for recovery do not contaminate the samples.

**Container No. 1 (Sample Filter)**

Remove filter from the filter holder; Place it in the labeled petri dish container. Seal the petri dish. See the Figure – 2

**Container No. 2 (Probe Rinse)**

Rinse the probe nozzle and fitting, probe liner, and front-half of the filter holder



thoroughly with a total of 100 ml of 0.1 N  $\text{HNO}_3$ , and place the wash into a sample storage container. Use of a total 100 ml is necessary for the subsequent blank correction procedures. Put the mark on the storage container for the fluid level to determine leakage during transportation. See the figure – 2

Container No. 3 (Impingers 1 through 3, Moisture Knockout Impinger when used,  $\text{HNO}_3$  /  $\text{H}_2\text{O}_2$  Impingers Contents and Rinses)

Measure the liquid in the first three impingers to within 0.5 ml using a graduated cylinder. Record the volume. This information is required to calculate the moisture content of the sampled flue gas.

Clean each of the first three impingers, the filter support, the back half of the filter housing, and connecting glassware by thoroughly rinsing with exactly 100 ml of 0.1 N  $\text{HNO}_3$ . Mark the height of the fluid level, seal and label the contents. See Figure 2.1

#### **Container Nos.4A (0.1 N $\text{HNO}_3$ )**

- Measure the volume of impinger No 4
- Place the liquid in Container No 4A. Rinse the impinger with exactly 100 ml of 0.1 N
- Place this rinse into the same Container No 4A.

#### **4B ( $\text{KMnO}_4$ / $\text{H}_2\text{SO}_4$ absorbing solution)**

- Pour all the solution of 5th & 6th impinger into the container No 4B. Measure the volume to within 0.5 ml
- Rinse the impingers (5th & 6th ) with exactly 100 ml of fresh acidifying  $\text{KMnO}_4$  solution into for all rinses (Approximately 33 ml per rinse).
- Similarly, use 100 ml distilled water for the rinsing of 5th & 6th impingers and connecting glass minimum three times, pour this rinses into the container No 4B.
- Don't fill these bottle completely, Take precaution to relive excess pressure.

#### **4C (8 N HCl rinse and dilution)**

- Remove the residue of Impinger No 5th & 6th with exactly 25 ml 8N HCl.
- Place this wash into different container ie 4C which contain 200 ml of water.
- Mark the container for fluid level. (See Figure – 2.2)

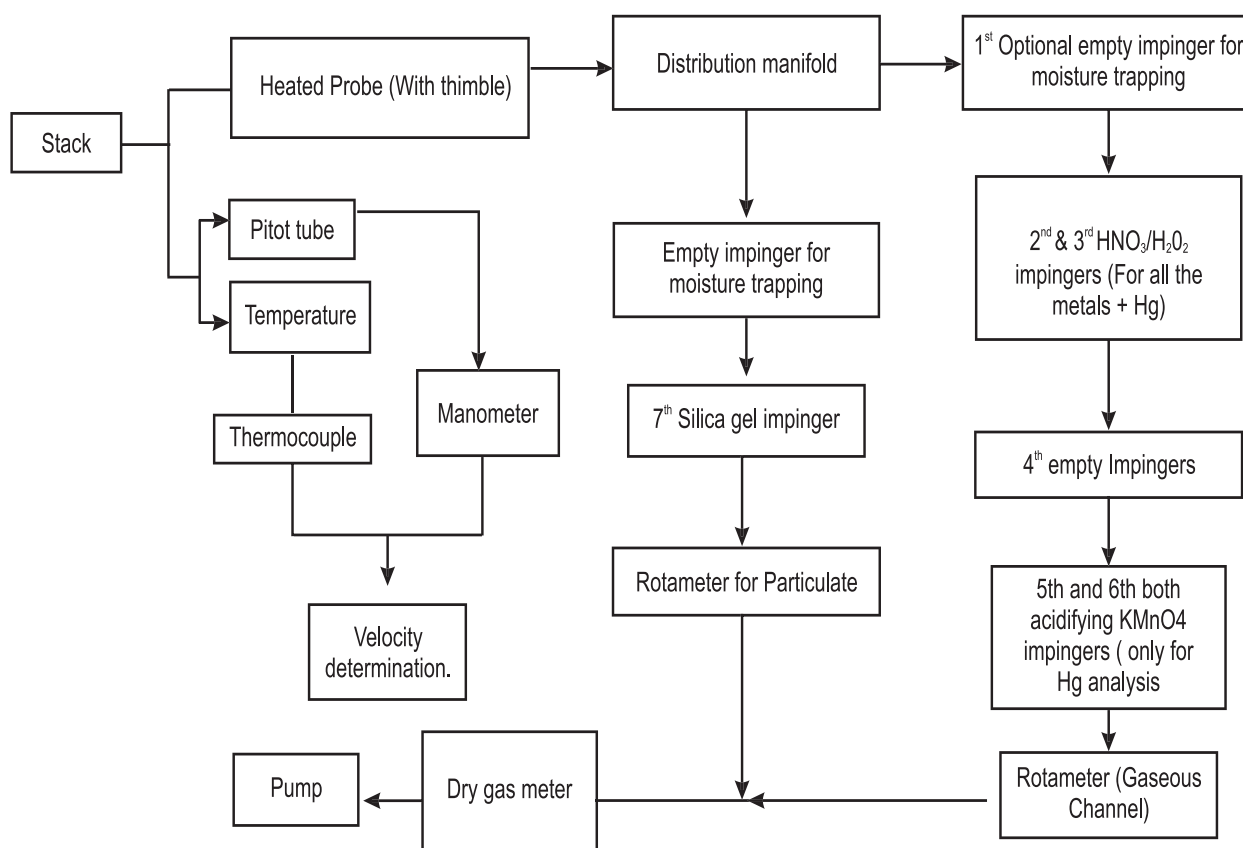
#### **Container No. 5 (Silica Gel)**

- Transfer the silica gel from its impinger to its original container and seal it.

- If a balance is available in the field, record the weight of the spent silica gel (or silica gel plus impinger) to the nearest 0.5 g.

**Container No. 6A (0.1 N HNO<sub>3</sub> Blank)**

- Container No. 6B (Water Blank).
- Container No. 7 (5 Percent HNO<sub>3</sub> /10 Percent H<sub>2</sub>O<sub>2</sub> Blank).
- Container No. 8 (Acidified KMnO<sub>4</sub> Blank).
- Container No. 9 (8 N HCl Blank).
- Container No. 10 (Sample Filter Blank).



**Figure - 1: Sampling Train for Metals and Non Metals**

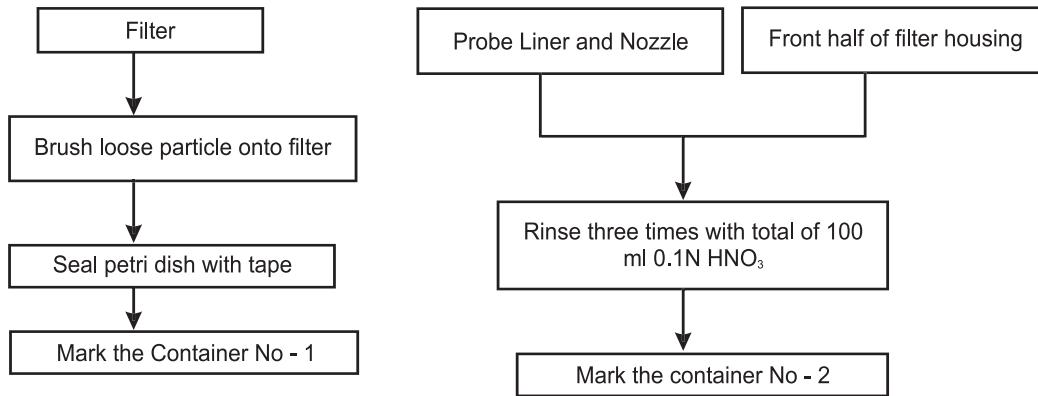


Figure -2: Sample Recovery Scheme for Sample filter, Probe rinse, Front half the filter housing

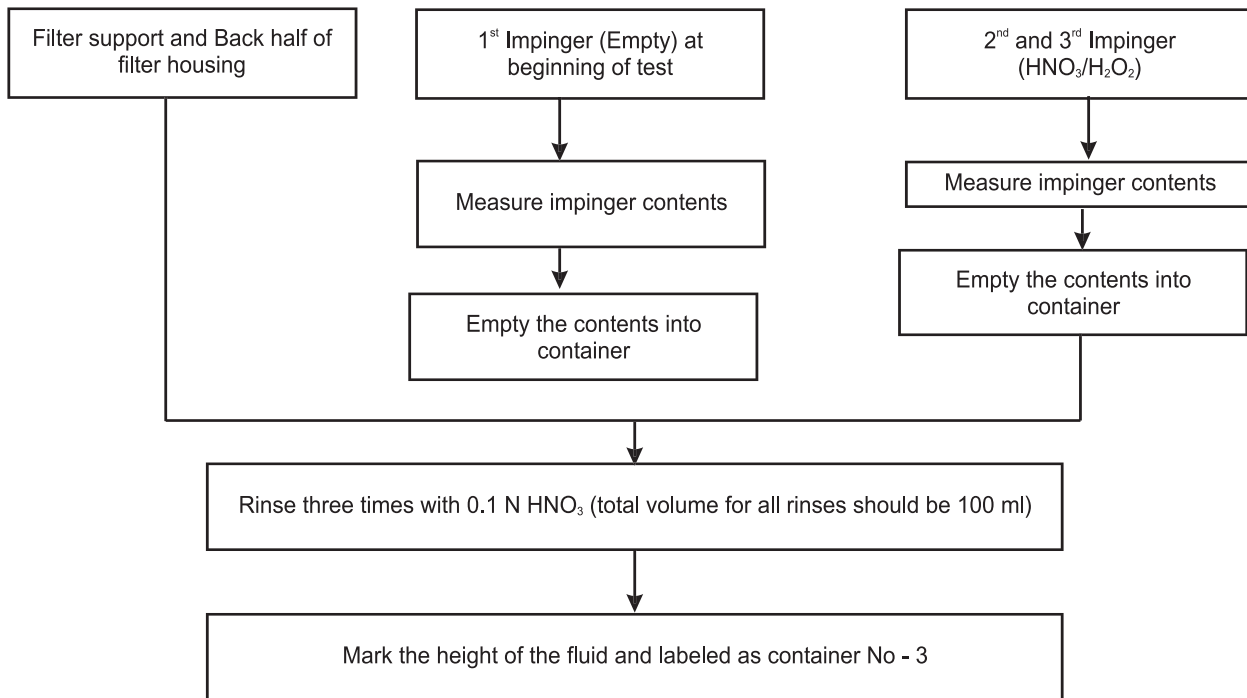
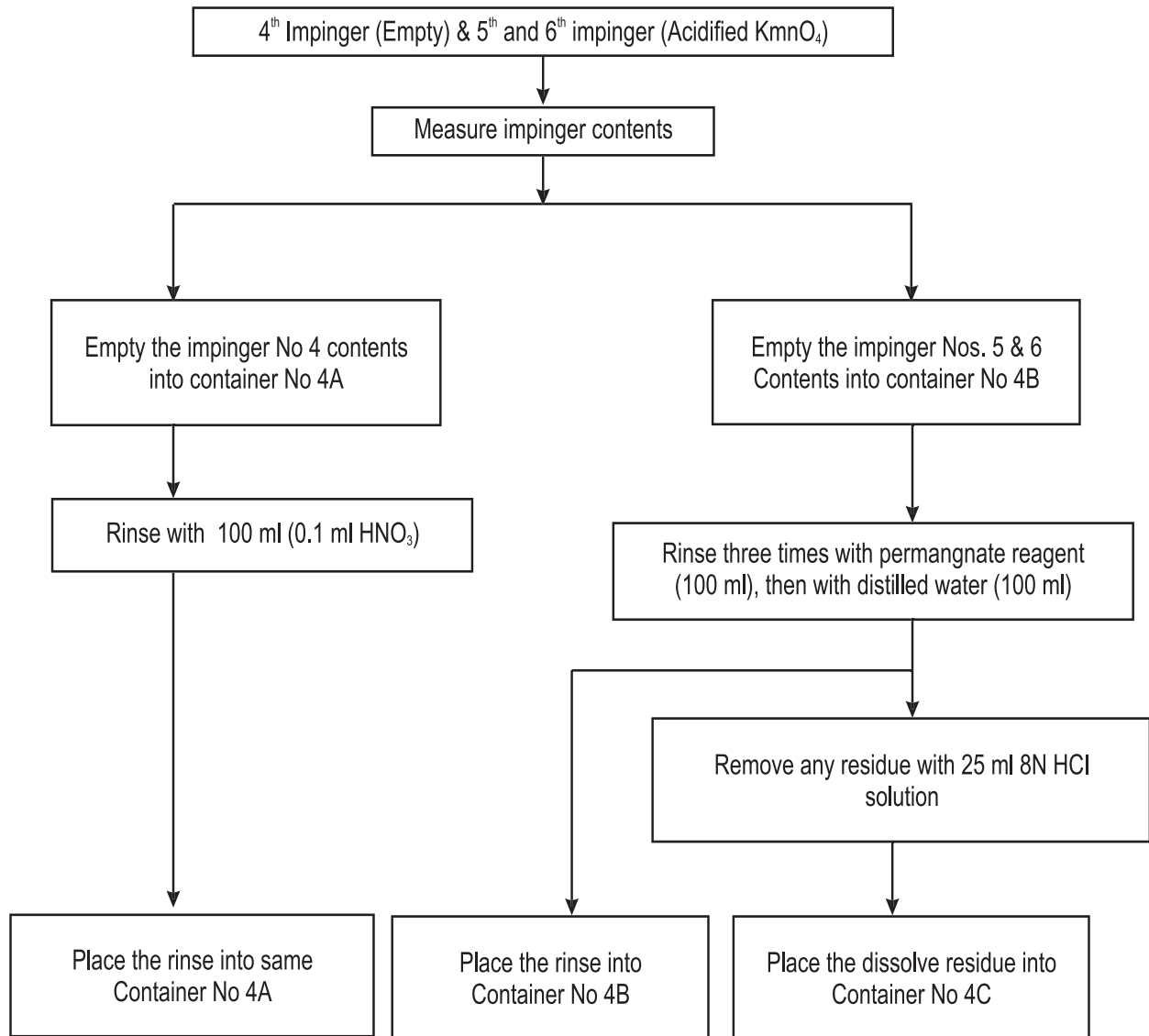


Figure -2.1: Sample Recovery Scheme for Filter support and Back half of filter housing, 1<sup>st</sup>(Empty), 2<sup>nd</sup>, 3<sup>rd</sup> Impinger (HNO<sub>3</sub>/H<sub>2</sub>O<sub>2</sub>)



**Figure-2.2: Sample Recovery Scheme 4<sup>th</sup> Impinger (Empty) & 5<sup>th</sup> and 6<sup>th</sup> Impinger (Acidified KmnO<sub>4</sub>)**

**Table - 2**  
**Sample detail sheet**

**Industry Name & Address:**  
**Date & Time of Sampling**

| Container No     | Sample Information   | Volume/wight the sample | Remartks |
|------------------|--|-------------------------|----------|
| Container No. 1  | Filter and any particulate matter or filter fiber that adhere to the filter holder gasket keep them into container no 1.   |                         |          |
| Container No. 2  | Rinse probe nozzle and fitting, liner and nozzle, front half of filter housing by 100 ml of 0.1N HNO <sub>3</sub> Place this rinses in Container no 2  |                         |          |
| Container No. 3  | Solution of 1 throught 3 impingers pour it in container 3. Clean each of the first three impingers, the filter support, the back half of the filter housing, and connecting glassware by thoroughly rinsing with exactly 100 ml of 0.1N HNO <sub>3</sub> , pour this rinses in the same container. |                         |          |
| Container No. 4A | Liquid of impinger No 4 as well as rinsing solution (100 ml of 0.1N HNO <sub>3</sub> ) of the same impinger keep in the container No 4A.   |                         |          |
| Container No. 4B | It contains solution of both the 5 <sup>th</sup> & 6 <sup>th</sup> Impingers (Acidifying permanganate impinger) as well as rinsing solution (100 ml of fresh acidified KMnO <sub>4</sub> &100 ml of distilled water) of same impingers.  |                         |          |
| Container No. 4C | If deposits remain in the 5 <sup>th</sup> & 6 <sup>th</sup> impingers, wash them with exactly 25 ml 8N HCl & pour this washing liquid into container No 4C containing 200 ml of water.   |                         |          |
| Container No. 5  | Note the color of the indicating silica gel and transfer the silica gel from its impinger to container No 5.   |                         |          |
| Container No. 6A | Keep blank of 0.1N HNO <sub>3</sub> (used in the sample recovery process) into container No A.   |                         |          |
| Container No. 6B | Water Blank (water used for the sample recovery): Keep water blank into container No 6B.   |                         |          |
| Container No. 7  | Keep blank of Nitric acid impinger reagent (5 Percent HNO <sub>3</sub> /10 Percent H <sub>2</sub> O <sub>2</sub> ) into the container 7  |                         |          |
| Container No. 8  | Blank of Acidified KMnO <sub>4</sub> impinger solution pour in to container No 8   |                         |          |
| Container No. 9  | Keep blank of 8N HCl (sample recovery reagent) in to Container No. 9   |                         |          |
| Container No. 10 | Sample Filter Blank i.e. unused filter from the same lot as the sampling filters.  |                         |          |

*Note: volume of the blank subjected, to be decided according to the volume of sample (to be considered for the analysis).*

**Table - 3  
Field Data Sheet**

**Name & Address**  
**Date & time of sampling**  
**Ambient temperature °C**  
**Barometric Pressure (mm mercury column)**  
**Moisture in the flue gas (%) flue gas composition (CO<sub>2</sub> %, O<sub>2</sub> %,N<sub>2</sub>)**  
**Filter No and weight ( Initial as well as Final)**

| Travers Point | ΔP (mm) | Ts (°K) | Ps | Us (m/s) | Qs (m <sup>3</sup> /hr) | Rs (LPM) | P <sub>m</sub>  |                 | Rm (LPM) | Time (min) | DGM (M <sup>3</sup> ) |       | V <sub>std</sub> (Nm <sup>3</sup> ) |
|---------------|---------|---------|----|----------|-------------------------|----------|-----------------|-----------------|----------|------------|-----------------------|-------|-------------------------------------|
|               |         |         |    |          |                         |          | P <sub>m0</sub> | P <sub>m1</sub> |          |            | Initial               | Final |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |
|               |         |         |    |          |                         |          |                 |                 |          |            |                       |       |                                     |

ΔP = Stack Gas Velocity Pressure, (mm water column), Ts = Stack temperature (°K)  
 Ps = Static pressure (mm water column), Us = Velocity of stack gas (m/s),  
 Qs = Volumetric Flow rate / discharge, Rs = Flow at nozzle (LPM),  
 Pm = Vacuum Pressure Drop (mm mercury column),  
 Rm = Determination of sampling rate at gas meter. (LPM),  
 Vstd = Determination of volume of gas sampled

**Other required information:**

- o Feed rate of hazardous waste
- o The nature, composition and quantity of the material being incinerated during monitoring
- o Installed and operating capacity of the incinerator
- o No of sampling ports
- o Internal diameter of the stack
- o Nozzle size selected for sampling
- o Pitot tube constant
- o ID fan capacity
- o Pollution control equipment installed and its status
- o House keeping

**Signature of sample collector**      **Verified by**      **Approved by**      **Occupier/  
Representative of  
the incinerator facility**

## Part-II

### STANDARD OPERATING PROCEDURE (SOP) OF SAMPLE PREPARATION FOR ANALYSIS OF METALS AND NON METALS

#### 1.0 Sample Preparation

Note the level of the liquid in each of the containers and determine if any sample was lost during shipment. A diagram illustrating sample preparation and analysis procedures for each of the sample train components is shown in Figure –3 and Figure – 3.1. By difference in weight and gas sample volume (Field data) calculates Particulate Matter concentration in mg/Nm<sup>3</sup>.

#### Container No. 1 (Sample Filter)

If particulate emissions are being determined, first desiccate the filter and filter catch without added heat (do not heat the filters to speed the drying) and weigh to a constant weight.

#### Option I – Microwave digestion

- Make pieces of filter papers/ thimbles (Do not use metallic scissor).
- Place the pieces of in the analyst's choice of either individual microwave pressure relief vessels or Parr R Bombs.
- Add 6 ml of concentrated HNO<sub>3</sub> and 4 ml of concentrated HF to each vessel
- In microwave heat the sample for 2- 3 min, then turn off the microwave for 2 to 3 minutes and heat for 2 – 3 minutes again
- Continue this alteration until the 12 to 15 minutes. This procedure should comprise approximately 24 to 30 minutes at 600 watts.

#### Option II – Hot Plate Digestion

- Place the pieces of thimbles in acid cleaned Teflon beaker add about 50 ml distilled water,
- Add 6 ml of concentrated HNO<sub>3</sub> and 4 ml of concentrated HF to it.
- Place it on hot plate under fume extraction hood.
- Set the Temperature at 70 °C. Continue to digest for 12 hrs.

#### Container No. 2 (Probe Rinse)

- Verify that the pH of this sample is 2 or lower. If it is not, acidify the sample by careful addition with stirring of concentrated HNO<sub>3</sub> to pH 2.
- Use water to rinse the sample into a Teflon beaker, and cover the beaker with a ribbed watch glass. Reduce the sample volume to approximately 20 ml by heating on a hot plate at a temperature below boiling.

- Add 6 ml of concentrated  $\text{HNO}_3$  and 4 ml of concentrated HF to it. Place it on hot plate under fume extraction hood. Set the Temperature at 70 °C continue the digestion for 12 hrs.
- If the sampling train includes an optional glass cyclone in front of the filter, prepare and digest the cyclone catch by the same way.
- Then combine the resultant sample directly with the acid digested portions of the filter prepared previously, acid rinse concentrate and cyclone catch concentrate (If done).
- Filter the combined sample using Whatman 41 filter paper. Dilute to 300 ml (or the appropriate volume for the expected metals concentration) with water.
- This diluted sample is "Analytical Fraction 1". Measure and record the volume of Analytical Fraction 1 to within 0.1 ml.
- Quantitatively remove a 50-ml aliquot and label as "Analytical Fraction 1B". Label the remaining 250-ml portion as "Analytical Fraction 1A". Analytical Fraction 1A is used for ICAP or AAS analysis for all desired metals except Hg.
- Analytical Fraction 1B is used for the determination of front-half Hg. This fraction should be treated with acid and  $\text{KMnO}_4$  at 90°C for 2 hours.
- Excess  $\text{KMnO}_4$  should be removed by using Hydroxylamine Hydrochloride before analysis of Hg.

### **Container No.3 (Impingers 1-3)**

- Measure and record the total volume of this sample to within 0.5 ml, if the leakage found significant make up with fresh distilled water.
- Remove a 75- to 100-ml aliquot for Hg analysis and label the aliquot "Analytical Fraction 3B".
- Label the remaining portion as "Sample Fraction 3A".
- Verify that the pH of Sample Fraction 3A is 2 or lower. If necessary, use concentrated  $\text{HNO}_3$  by careful addition and stirring to lower the pH upto 2.
- Use water to rinse Sample Fraction 3A into a beaker and then cover the beaker with a ribbed watch glass.
- Reduce Sample (3A) to approximately 20 ml by heating on a hot plate at a temperature just below boiling.
- Add 30 ml of 50 percent  $\text{HNO}_3$  and heat for 30 minutes on a hot plate to just below boiling.
- Add 10 ml of 3 percent  $\text{H}_2\text{O}_2$  and heat for 10 more minutes. Add 50 ml of hot water, and heat the sample for an additional 20 minutes. Cool, filter the sample, and dilute to



150 ml (or the appropriate volume for the expected metals concentrations) with water. Analytical Fraction 3A is analyzed for all metals except Hg.

- Analytical fraction 3B will be digested separately with HCl and  $\text{KMnO}_4$  at 90 °C for two hours. Excess Permanganate should be removed by Hydrxylamine Hydrochloride before analysis in Cold Vapour AAS.

Container No. 4A (Empty impinger washing liquid with 0.1 N  $\text{HNO}_3$ ), 4B ( $\text{KMnO}_4$  /  $\text{H}_2\text{SO}_4$  absorbing solution of impinger 5 and 6), and 4C (8 N HCl rinse of impinger 5 and 6 for scaling of  $\text{MnO}_2$ ) Keep the samples in Containers Nos. 4A, 4B, and 4C separate from each other. Measure and record the volume of 4A to within 0.5 ml.

Concentrate the sample upto 20 ml on hot plate at below boiling temperature. Keep it separate. To remove any brown  $\text{MnO}_2$  precipitate from the contents of Container No. 4B, filter its contents through Whatman 40 filter paper into a 500 ml volumetric flask, make up the volume with distilled water. This fraction is analytical fraction 4B.

Save the filter for digestion of the brown  $\text{MnO}_2$  precipitate. Place the saved filter into an appropriately sized vented container, which will allow release of any gases including chlorine formed when the filter is digested in a laboratory hood. Add 25 ml of 8 N HCl to the filter and allow to digest for a minimum of 24 hours at room temperature. Filter the contents of Container No. 4C through a Whatman 40 filter into a 500-ml volumetric flask. Then filter the resultant solution of the digestion of the brown  $\text{MnO}_2$  from Container No. 4B through another Whatman 40 filter into the same 500-ml volumetric flask, finally dilute and mix well to volume with water. Discard the Whatman 40 filter. Mark this combined 500-ml dilute HCl solution as Analytical fraction 4C. So three samples will be generated in this section for Hg analysis. All these fractions shall be digested and concentrated to desired volume with HCl and  $\text{KMnO}_4$  at 90 °C for two hours. Excess Permanganate should be removed by Hydrxylamine Hydrochloride before analysis in Cold Vapour AAS.

## 5.1 Sample Analysis

For each sampling train sample run, seven individual analytical samples are generated; two (Analytical fraction 1A and 3A) for all desired metals except Hg, and five for Hg (Analytical fraction 1B, 3B, 4A, 4B and 4C). A schematic identifying each sample container and the prescribed analytical preparation and analysis scheme is shown in Figure 3 and Figure 3.1 Blanks for all reagents used should be processed with samples in parallel.

## 6.0 CALCULATIONS

For Molecular weight determination, Stack gas velocity, Isokinetic Flow rate, Moisture content and parameters required for particulate emission calculation follow the formulae mentioned in method prescribed for particulate matter determination.

Dry Gas Volume. Using the data from this test, calculate V, the dry gas sample volume at standard conditions  $m(\text{std})$  as outline Correct the sample volume measured by the dry gas meter to standard conditions (25 °C, 760 mm Hg or 68 °F, 29.92in. Hg) by using following Equation. Where, Y is DGM Calibration Factor.

$$V_{mstd} = V_m \cdot Y \left[ \frac{T_{std}}{T_m} \right] \left[ \frac{P_{bar}}{P_{std}} \right] = K_1 \cdot Y \cdot V_m \left[ \frac{P_{bar}}{P_m} \right]$$

Where:

$K_1$  = 0.3858 °K/mm Hg for metric units,  
= 17.64 °C/in. Hg for English units

$P_{bar}$  = Barometric pressure at the exit orifice of the DGM, mm Hg (in. Hg).

$P_{std}$  = Standard absolute pressure, 760 mm Hg (29.92 in.Hg).

$T_m$  = Average DGM absolute temperature, °K (°C).

$T_{std}$  = Standard absolute temperature, 293 °K

$Y$  = Dry gas meter calibration factor

$V_{m(std)}$  = Dry gas volume measured by the dry gas meter, corrected to standard conditions,  $Nm^3$

$V_m$  = {Sampling rate in gas channel (LPM) X duration (Minutes)} / 1000  $m^3$ .

Calculate all the seven fraction (2 for other metals and 5 for mercury) in mass of individual elements following the formula

### Metals (Except Hg) in Source Sample

$$M_x = C_x \text{ (ppm)} * D * V_{ds}$$

Where:

$M_x$  = Total mass of each metal in  $\mu g$ .

$C_x$  = Concentration of metal in respective fraction as read from the standard curve in  $\mu g/ml$  (ppm) after respective blank subtraction

$D$  = dilution Factor

$V_{ds}$  = Total volume of digested sample solution in Analytical fraction ml.

$M_x$  values calculated for fraction 1A and 3A should be added individually to represent to total mass for each metals except Hg. The concentration emitted from stack would be calculated as below.

$$\{M_x(1A) + M_x(3A)\} * 10^{-3} / V_{m(std)} \text{ mg}/Nm^3$$

### Similarly for Hg

$$\{M_x(1B) + M_x(3B) + M_x(4A) + M_x(4C)\} * 10^{-3} / V_{m(std)} \text{ mg}/Nm^3$$

*Note: Report concentration as corrected at 11%  $O_2$  (as mentioned in the method for PM determination)*

## Determination of Sulfur Dioxide Emissions from Stationary Sources

### 1. PRINCIPLE AND APPLICABILITY

#### 1.1 Principle

A gas sample is extracted from the sampling point in the stack. The sulfuric acid mist (including sulfur trioxide) and the sulfur dioxide (SO<sub>2</sub>) are separated. The SO<sub>2</sub> fraction is measured by the barium-thorin titration method.

#### 1.2 Applicability & Interferences

##### 1.2.1 Applicability

This method is applicable for the determination of SO<sub>2</sub> emissions from stationary sources. The minimum detectable limit of the method has been determined to be 3.4 mg of SO<sub>2</sub> /m<sup>3</sup> ( $2.12 \times 10^{-7}$  lb/ft<sup>3</sup>). Although no upper limit has been established, tests have shown that concentrations as high as 80,000 mg/m<sup>3</sup> of SO<sub>2</sub> can be collected efficiently in two midjet impingers, each containing 15 ml of 3 percent hydrogen peroxide, at a rate of 1.0 liter/min for 20 minutes. Based on theoretical calculations, the upper concentration limit in a 20-liter sample is about 93,300 mg/m<sup>3</sup>.

##### 1.2.2 Interferences

Possible interferants are free ammonia, water-soluble cations, and fluorides. The cations and fluorides are removed by glass wool filters and an isopropanol bubbler, and hence do not affect the SO<sub>2</sub> analysis. When samples are being taken from a gas stream with high concentrations of very fine metallic fumes (such as found in inlets to control devices), a high-efficiency glass fiber filter must be used in place of the glass wool plug (i.e., the one in the probe) to remove the cation interferants.

Free ammonia interferes by reacting with SO<sub>2</sub> to form particulate sulfite and by reacting with the indicator.

### 2. APPARATUS

#### 2.1 Sampling.

##### 2.1.1 Sampling Train

The sampling train is shown in Figure 6-1, and component parts are discussed below. The tester has the option of substituting sampling equipment described in Method 8 in place of

the midget impinger equipment of Method 6. However, the Method 8 train must be modified to include a heated filter between the probe and isopropanol impinger, and the operation of the sampling train and sample analysis must be at the flow rates and solution volumes defined in Method 8.

The tester also has the option of determining SO<sub>2</sub> simultaneously with particulate matter and moisture determinations by (1) replacing the water in Method 5 impinger system with 3 percent peroxide solution, or (2) by replacing the Method 5 water impinger system with a Method 8 isopropanol-filter-peroxide system. The analysis for SO<sub>2</sub> must be consistent with the procedure of Method 8.

### 2.1.1.1 Probe

Borosilicate glass, or stainless steel approximately 6-mm inside diameter, with a heating system to prevent water condensation and a filter (either in-stack or heated out-stack) to remove particulate matter, including sulfuric acid mist. A plug of glass wool is a satisfactory filter.

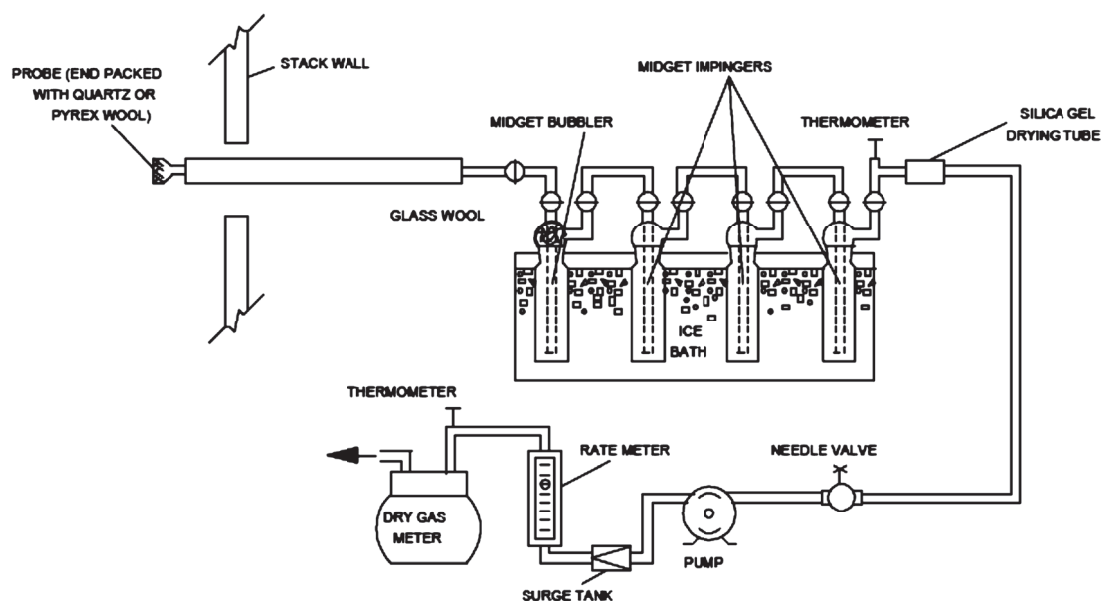


Figure 6-1. SO<sub>2</sub> Sampling Train

### 2.1.1.2 Bubbler and Impingers

One midget bubbler, with medium-coarse glass frit and borosilicate or quartz glass wool packed in top (see Figure 6-1) to prevent sulfuric acid mist carryover, and three 30-ml midget

impingers. The bubbler and midget impingers must be connected in series with leak-free glass connectors. Silicone grease may be used, if necessary, to prevent leakage.

At the option of the tester, a midget impinger may be used in place of the midget bubbler. Other collection absorbers and flow rates may be used, but the collection efficiency must be shown to be at least 99 percent for each test run and must be documented in the report. If the efficiency is found to be acceptable after a series of three tests, further documentation is not required. To conduct the efficiency test, an extra absorber must be added and analyzed separately. This extra absorber must not contain more than 1 percent of the total SO<sub>2</sub>.

#### **2.1.1.2 Glass Wool**

Borosilicate or quartz.

#### **2.1.1.3 Stopcock Grease**

Acetone-insoluble, heat-stable silicone grease may be used, if necessary.

#### **2.1.1.4 Temperature Gauge**

Dial thermometer, or equivalent, to measure temperature of gas leaving impinger train to within 1° C (2° F).

#### **2.1.1.5 Drying Tube**

Tube packed with 6- to 16-mesh indicating-type silica gel, or equivalent, to dry the gas sample and to protect the meter and pump. See also the note in Method 5, Section 3.1.2.

#### **2.1.1.6 Valve**

Needle valve, to regulate sample gas flow rate.

#### **2.1.1.7 Pump**

Leak-free diaphragm pump, or equivalent, to pull gas through the train. Install a small surge tank between the pump and rate meter to eliminate the pulsation effect of the diaphragm pump on the rotameter.

#### **2.1.1.8 Rate Meter**

Rotameter, or equivalent, capable of measuring flow rate to within 2 percent of the selected flow rate of about 1000 cc/min.

#### **2.1.1.9 Volume Meter**

Dry gas meter (DGM), sufficiently accurate to measure the sample volume to within 2 percent, calibrated at the selected flow rate and conditions actually encountered during sampling, and equipped with a temperature gauge (dial thermometer, or equivalent) capable of measuring temperature accurately to within 3 °C (5.4 °F).

### **2.1.1.10 Barometer**

Mercury, aneroid, or other barometer capable of measuring atmospheric pressure to within 2.5 mm (0.1 in.)Hg.

### **2.1.1.11 Vacuum Gauge and Rotameter**

At least 760-mm (30-in.) Hg gauge and 0— to 40-cc/min rotameter, to be used for leak-check of the sampling train.

## **2.2 Materials required for Sample Recovery**

### **2.2.1 Wash Bottles.**

Polyethylene or glass, 500-ml, two.

### **2.2.2 Storage Bottles.**

Polyethylene, 100-ml, to store impinger samples (one per sample).

## **2.3 Materials and instruments required for Analysis.**

### **2.3.1 Pipettes**

Volumetric type, 5-ml, 20-ml (one per sample), and 25-ml sizes

### **2.3.2 Volumetric Flasks**

100-ml size (one per sample) and 1000-ml size.

### **2.3.3 Burettes**

5-ml and 50-ml sizes.

### **2.3.4 Erlenmeyer Flasks**

250-ml size (one for each sample, blank, and standard).

### **2.3.5 Dropping Bottle**

125-ml size, to add indicator.

### **2.3.6 Graduated Cylinder**

100-ml size.

### **2.3.7 Spectrophotometer**

To measure absorbance at 352 nanometers.

### **3. REAGENTS**

Unless otherwise indicated, all reagents must conform to the specifications established by the Committee on Analytical Reagents of the American Chemical Society. Where such specifications are not available, use the best available grade.

#### **3.1 Sampling**

##### **3.1.1 Water**

Deionized distilled to conform to ASTM Specification D 1193—77, Type 3. At the option of the analyst, the KMnO<sub>4</sub> test for oxidizable organic matter may be omitted when high concentrations of organic matter are not expected to be present.

##### **3.1.2 Isopropanol, 80 Percent**

Mix 80 ml of isopropanol with 20 ml of water.

**3.1.2.1** Check each lot of isopropanol for peroxide impurities as follows: Shake 10 ml of isopropanol with 10 ml of freshly prepared 10 percent potassium iodide solution. Prepare a blank by similarly treating 10 ml of water. After 1 minute, read the absorbance at 352 nanometers on a spectrophotometer, using a 1-cm path length. If absorbance exceeds 0.1, reject alcohol for use.

**3.1.2.2** Peroxides may be removed from isopropanol by redistilling or by passage through a column of activated alumina; however, reagent grade isopropanol with suitably low peroxide levels may be obtained from commercial sources. Rejection of contaminated lots may, therefore, be a more efficient procedure.

##### **3.1.3 Hydrogen Peroxide, 3 Percent**

Dilute 30 percent hydrogen peroxide 1:9 (v/v) with water (30 ml is needed per sample). Prepare fresh daily.

##### **3.1.4 Potassium Iodide Solution, 10 Percent**

Dissolve 10.0 g of KI in water, and dilute to 100 ml. Prepare when needed.

#### **3.2 Sample Recovery**

##### **3.2.1 Water**

Same as in Section 3.1.1.

##### **3.2.2 Isopropanol, 80 Percent**

Same as in Section 3.1.2.

#### **3.3 Chemicals & Reagent required for Analysis**

### 3.3.1 Water

Same as in Section 3.1.1.

### 3.3.2 Isopropanol, 100 Percent

### 3.3.3 Thorin Indicator

1-(o-arsenophenylazo)-2-naphthol-3,6-disulfonic acid, disodium salt, or equivalent. Dissolve 0.20 g in 100 ml of water.

### 3.3.4 Barium Standard Solution, 0.0100 N

Dissolve 1.95 g of barium perchlorate trihydrate [Ba(ClO<sub>4</sub>)<sub>2</sub> · 3H<sub>2</sub>O] in 200 ml water, and dilute to 1 liter with isopropanol. Alternatively, 1.22 g of barium chloride dihydrate [BaCl<sub>2</sub> · 2H<sub>2</sub>O] may be used instead of the perchlorate. Standardize as in Section 5.5.

### 3.3.5 Sulfuric Acid Standard, 0.0100 N

Purchase or standardize to  $\pm 0.0002$  N against 0.0100 N NaOH which has previously been standardized against potassium acid phthalate (primary standard grade).

## 4. PROCEDURE

### 4.1 Sampling.

#### 4.1.1 Preparation of Collection Train

Measure 15 ml of 80 percent isopropanol into the midget bubbler and 15 ml of 3 percent hydrogen peroxide into each of the first two midget impingers. Leave the final midget impinger dry. Assemble the train as shown in Figure 6-1. Adjust probe heater to a temperature sufficient to prevent water condensation. Place crushed ice and water around the impingers.

#### 4.1.2 Leak-Check Procedure

A leak-check prior to the sampling run is optional; however, a leak-check after the sampling run is mandatory. The leak-check procedure is as follows:

- Temporarily attach a suitable (e.g., 0- to 40-cc/min) rotameter to the outlet of the DGM, and place a vacuum gauge at or near the probe inlet. Plug the probe inlet, pull a vacuum of at least 250 mm (10 in.) Hg, and note the flow rate as indicated by the rotameter. A leakage rate not in excess of 2 percent of the average sampling rate is acceptable. Note: Carefully release the probe inlet plug before turning off the pump.
- It is suggested (not mandatory) that the pump be leak-checked separately, either prior to or after the sampling run. If done prior to the sampling run, the pump leak-check shall precede the leak-check of the sampling train described immediately above; if done after



the sampling run, the pump leak check shall follow the train leak-check. To leak-check the pump, proceed as follows: Disconnect the drying tube from the probe-impinger assembly. Place a vacuum gauge at the inlet to either the drying tube or the pump, pull a vacuum of 250 mm (10 in.) Hg, plug or pinch off the outlet of the flow meter, and then turn off the pump. The vacuum should remain stable for at least 30 seconds.

#### **4.1.3 Sample Collection.**

- Record the initial DGM reading and barometric pressure. To begin sampling, position the tip of the probe at the sampling point, connect the probe to the bubbler, and start the pump. Adjust the sample flow to a constant rate of approximately 1.0 liter/min as indicated by the rotameter. Maintain this constant rate ( $\pm 10$  percent) during the entire sampling run. Take readings (DGM, temperatures at DGM and at impinger outlet, and rate meter) at least every 5 minutes. Add more ice during the run to keep the temperature of the gases leaving the last impinger at 20 °C (68 °F) or less. At the conclusion of each run, turn off the pump, remove probe from the stack, and record the final readings. Conduct a leak-check as in Section 4.1.2. (This leak-check is mandatory.) If a leak is found, void the test run or use procedures acceptable to the Administrator to adjust the sample volume for the leakage. Drain the ice bath, and purge the remaining part of the train by drawing clean ambient air through the system for 15 minutes at the sampling rate.
- Clean ambient air can be provided by passing air through a charcoal filter or through an extra midjet impinger with 15 ml of 3 percent H<sub>2</sub>O<sub>2</sub>. The tester may opt to use simply ambient air without purification.

#### **4.2 Sample Recovery**

Disconnect the impingers after purging. Discard the contents of the midjet bubbler. Pour the contents of the midjet impingers into a leak-free polyethylene bottle for shipment. Rinse the three midjet impingers and the connecting tubes with water, and add the washings to the same storage container. Mark the fluid level. Seal and identify the sample container.

#### **4.3 Sample Analysis.**

- Note level of liquid in container, and confirm whether any sample was lost during shipment; note this on analytical data sheet.
- Transfer the contents of the storage container to a 100-ml volumetric flask, and dilute to exactly 100 ml with water. Pipette a 20-ml aliquot of this solution into a 250-ml Erlenmeyer flask, add 80 ml of 100 percent isopropanol and two to four drops of thiorin indicator, and titrate to a pink endpoint using 0.0100 N barium standard solution. Repeat,

and average the titration volumes. Run a blank with each series of samples. Replicate titrations must agree within 1 percent or 0.2 ml, whichever is larger.

Note: Protect the 0.0100 N barium standard solution from evaporation at all times.

#### **4.4 QC Sample Analysis.**

- Concurrently analyze the one/two Control samples in the same manner to evaluate the technique of the analyst and the standards preparation. (Note: It is recommended that known quality control samples be analyzed prior to the compliance and audit sample analysis to optimize the system accuracy and precision. One source of these samples is the Source Branch listed in Section 3.3.6.)
- Calculate the concentrations in mg/NM<sup>3</sup> using the specified sample volume in the audit instructions.
- The concentrations of the audit samples obtained by the analyst shall agree within 5 percent of the actual concentrations. If the 5-percent specification is not met, reanalyze the compliance samples and audit samples, and include initial and reanalysis values in the test report (see Note in first paragraph of this section).
- Failure to meet the 5-percent specification may require retests until the audit problems are resolved. However, if the audit results do not affect the compliance or noncompliance status of the affected facility, the Administrator may waive the reanalysis requirement, further audits, or retests and accept the results of the compliance test. While steps are being taken to resolve audit analysis problems, the Administrator may also choose to use the data to determine the compliance or noncompliance status of the affected facility.

### **5. CALIBRATION**

#### **5.1 Metering System.**

##### **5.1.1 Initial Calibration.**

- Before its initial use in the field, first leak-check the metering system (drying tube, needle valve, pump, rotameter, and DGM) as follows: Place a vacuum gauge at the inlet to the drying tube, and pull a vacuum of 250 mm (10 in.) Hg; plug or pinch off the outlet of the flow meter, and then turn off the pump. The vacuum shall remain stable for at least 30 seconds. Carefully release the vacuum gauge before releasing the flow meter end.
- Next, remove the drying tube, and calibrate the metering system (at the sampling flow rate specified by the method) as follows: Connect an appropriately sized wet test meter (e.g., 1 liter per revolution) to the inlet of the drying tube. Make three independent calibration runs, using at least five revolutions of the DGM per run. Calculate the calibration factor, Y

(wet test meter calibration volume divided by the DGM volume, both volumes adjusted to the same reference temperature and pressure), for each run, and average the results. If any Y-value deviates by more than 2 percent from the average, the metering system is unacceptable for use. Otherwise, use the average as the calibration factor for subsequent test runs.

### **5.1.2 Post-Test Calibration Check**

After each field test series, conduct a calibration check as in Section 5.1.1 above, except for the following variations

- (a) the leak-check is not to be conducted,
- (b) three, or more revolutions of the DGM may be used, and
- (c) only two independent runs need be made.

If the calibration factor does not deviate by more than 5 percent from the initial calibration factor determined in Section 5.1.1), then the DGM volumes obtained during the test series are acceptable. If the calibration factor deviates by more than 5 percent, recalibrate the metering system as in Section 5.1.1, and for the calculations, use the calibration factor (initial or recalibration) that yields the lower gas volume for each test run.

## **5.2 Thermometers**

Calibrate against mercury-in-glass thermometers.

## **5.3 Rotameter**

The rotameter need not be calibrated, but should be cleaned and maintained according to the manufacturer's instruction.

## **5.4 Barometer**

Calibrate against a mercury barometer.

## **5.5 Barium Standard Solution**

Standardize the barium perchlorate or chloride solution against 25 ml of standard sulfuric acid to which 100 ml of 100 percent isopropanol has been added. Run duplicate analyses. Calculate the normality using the average of a pair of duplicate analyses where the titrations agree within 1 percent or 0.2 ml, whichever is larger.

## **6. CALCULATIONS**

Carry out calculations, retaining at least one extra decimal figure beyond that of the acquired data. Round off figures after final calculation.

$C_{SO_2}$  = Concentration of  $SO_2$ , dry basis corrected to standard conditions, mg/dsm<sup>3</sup> (1b/dscf).

$N$  = Normality of barium standard titrant, meq./ml.

$P_{bar}$  = Barometric pressure at the exit orifice of the DGM, mm Hg (in. Hg).

$P_{std}$  = Standard absolute pressure, 760 mm Hg (29.92 in. Hg).

$T_m$  = Average DGM absolute temperature, °K (°R).

$T_{std}$  = Standard absolute temperature, 293 °K (528 °R).

$V_a$  = Volume of sample aliquot titrated, ml.

$V_m$  = Dry gas volume as measured by the DGM, dcm (dcf).

$V_{m(std)}$  = Dry gas volume measured by the DGM, corrected to standard conditions, dscm (dscf).

$V_{soln}$  = Total volume of solution in which the  $SO_2$  sample is contained, 100 ml.

$V_t$  = Volume of barium standard titrant used for the sample (average of replicate titrations), ml.

$V_{tb}$  = Volume of barium standard titrant used for the blank, ml.

$Y$  = DGM calibration factor.

32.03 = Equivalent weight of  $SO_2$ .

## 6.2 Dry Sample Gas Volume, Corrected to Standard Conditions.

$$V_{mstd} = V_m Y \left[ \frac{T_{std}}{T_m} \right] \left[ \frac{P_{bar}}{P_{std}} \right] = K_1 Y V_m \left[ \frac{P_{bar}}{P_m} \right] \quad \text{Eq. 6-1}$$

Where:

$K_1$  = 0.3858 °K/mm Hg for metric units,

= 17.64 °R/in. Hg for English units.

## 6.3 $SO_2$ Concentration.

$$C_{SO_2} = K_2 \frac{(V_t - V_{tb}) N \left[ \frac{V_{soln}}{V_a} \right]}{V_{m(std)}} \quad \text{Eq. 6-1}$$

$K_2$  = 32.03 mg/meq. for metric units,

=  $7.061 \times 10^{-5}$  lb/meq. for English units.

## 7.0 BIBLIOGRAPHY

1. Atmospheric Emissions from Sulfuric Acid Manufacturing Processes. U.S DHEW, PHS, Division of Air Pollution. Public Health Service Publication No. 999-AP-13. Cincinnati, OH. 1965.
2. Corbett, P.F. The Determination of SO<sub>2</sub> and SO<sub>3</sub> in Flue Gases. *Journal of the Institute of Fuel*. 24:237-243. 1961.
3. Matty, R.E. and E.K. Diehl. Measuring Flue-Gas SO<sub>2</sub> and SO<sub>3</sub>. *Power*. 101:94- 7. November 1957.
4. Patton, W.F. and J.A. Brink, Jr. New Equipment and Techniques for Sampling Chemical Process Gases. *J. Air Pollution Control Association*. 13:162. 1963.
5. Rom, J.J. Maintenance, Calibration, and Operation of Isokinetic Source- Sampling Equipment. Office of Air Programs, Environmental Protection Agency. Research Triangle Park, NC. APTD-0576. March 1972.
6. Hamil, H.F. and D.E. Camann. Collaborative Study of Method for the Determination of Sulfur Dioxide Emissions from Stationary Sources (Fossil- Fuel Fired Steam Generators). Environmental Protection Agency, Research Triangle Park, NC. EPA-650/4-74-024. December 1973.
7. Annual Book of ASTM Standards. Part 31; Water, Atmospheric Analysis. American Society for Testing and Materials. Philadelphia, PA. 1974. pp. 40-42.
8. Knoll, J.E. and M.R. Midgett. The Application of EPA Method 6 to High Sulfur Dioxide Concentrations. Environmental Protection Agency. Research Triangle Park, NC. EPA-600/4-76-038. July 1976.
9. Westlin, P. R. and R. T. Shigehara. Procedure for Calibrating and Using Dry Gas Volume Meters as Calibration Standards. *Source Evaluation Society Newsletter*. 3(1):17-30. February 1978.
10. Yu, K. K. Evaluation of Moisture Effect on Dry Gas Meter Calibration. *Source Evaluation Society Newsletter*. 5(1):24-28. February 1980.
11. Lodge, J.P., Jr., J.B. Pate, B.E. Ammons, and G.A. Swanson. The Use of Hypodermic Needles as Critical Orifices in Air Sampling. *J. Air Pollution Control Association*. 16:197-200. 1966
12. Shigehara, R.T., and Candace B. Sorrell. Using Critical Orifices as Method 5 Calibration Standards. *Source Evaluation Society Newsletter*. 10:4-15. August 1985.

# CHAPTER - 8

## Determination of Nitrogen Oxide Emissions from Stationary Sources

### 1. APPLICABILITY AND PRINCIPLE

#### 1.1 Applicability

This method is applicable to the measurement of nitrogen oxides emitted from stationary sources. The range of the method has been determined to be 2 to 400 milligrams NOX (as N<sub>2</sub>O) per dry standard cubic meter, without having to dilute the sample.

#### 1.2 Principle

A grab sample is collected in an evacuated flask containing a dilute sulfuric acid-hydrogen peroxide absorbing solution, and the nitrogen oxides, except nitrous oxide, are measured colorimetrically using the phenoldisulfonic acid (PDS) procedure.

### 2. APPARATUS

#### 2.1 Sampling (see Figure 7-1)

Other grab sampling systems or equipment, capable of measuring sample volume to within 2.0 percent and collecting a sufficient sample volume to allow analytical reproducibility to within 5 percent, will be considered acceptable alternatives. The following equipment is used in sampling:

##### 2.1.1 Probe

Borosilicate glass tubing, sufficiently heated to prevent water condensation and equipped with an in-stack or out-stack filter to remove particulate matter (a plug of glass wool is satisfactory for this purpose). Stainless steel or Teflon (Note: Mention of trade names or specific products does not constitute endorsement by U.S. EPA) tubing may also be used for the probe. Heating is not necessary if the probe remains dry during the purging period.

##### 2.1.2 Collection Flask

Two-liter borosilicate, round bottom flask, with short neck and 24/40 standard taper opening, protected against implosion or breakage.

##### 2.1.3 Flask Valve

T-bore stopcock connected to a 24/40 standard taper joint.

#### **2.1.4 Temperature Gauge**

Dial-type thermometer, or other temperature gauge, capable of measuring 1 °C (2 °F) intervals from -5 to 50 °C (25 to 125 °F).

#### **2.1.5 Vacuum Line**

Tubing capable of withstanding a vacuum of 75 mm (3 in.) Hg absolute pressure, with "T" connection and T-bore stopcock.

#### **2.1.6 Vacuum Gauge**

U-tube manometer, 1-meter (36-in.), with 1-mm (0.1-in.) divisions, or other gauge capable of measuring pressure to within 2.5 mm (0.10 in.) Hg.

#### **2.1.7 Pump**

Capable of evacuating the collection flask to a pressure equal to or less than 75 mm (3 in.) Hg absolute.

#### **2.1.8 Squeeze Bulb**

One-way

#### **2.1.9 Volumetric Pipette**

25-ml.

#### **2.1.10 Stopcock and Ground Joint Grease**

A high-vacuum, high-temperature chlorofluorocarbon grease is required. Halocarbon 25-5S has been found to be effective.

#### **2.1.11 Barometer**

Mercury, aneroid, or other barometer capable of measuring atmospheric pressure to within 2.5 mm (0.1 in.) Hg. See Note in Method 5, Section 2.1.9.

### **2.2 Sample Recovery**

The following equipment is required for sample recovery:

#### **2.2.1 Graduated Cylinder**

50-ml with 1-ml divisions.

#### **2.2.2 Storage Containers**

Leak-free polyethylene bottles.

### 2.2.3 Wash Bottle

Polyethylene or glass.

### 2.2.4 Glass Stirring Rod.

### 2.2.5 Test Paper for Indicating pH.

To cover the pH range of 7 to 14.

## 2.3 Analysis.

For the analysis, the following equipment is needed:

### 2.3.1 Volumetric Pipettes.

Two 1-ml, two 2-ml, one 3-ml, one 4-ml, two 10 ml, and one 25-ml for each sample and standard.

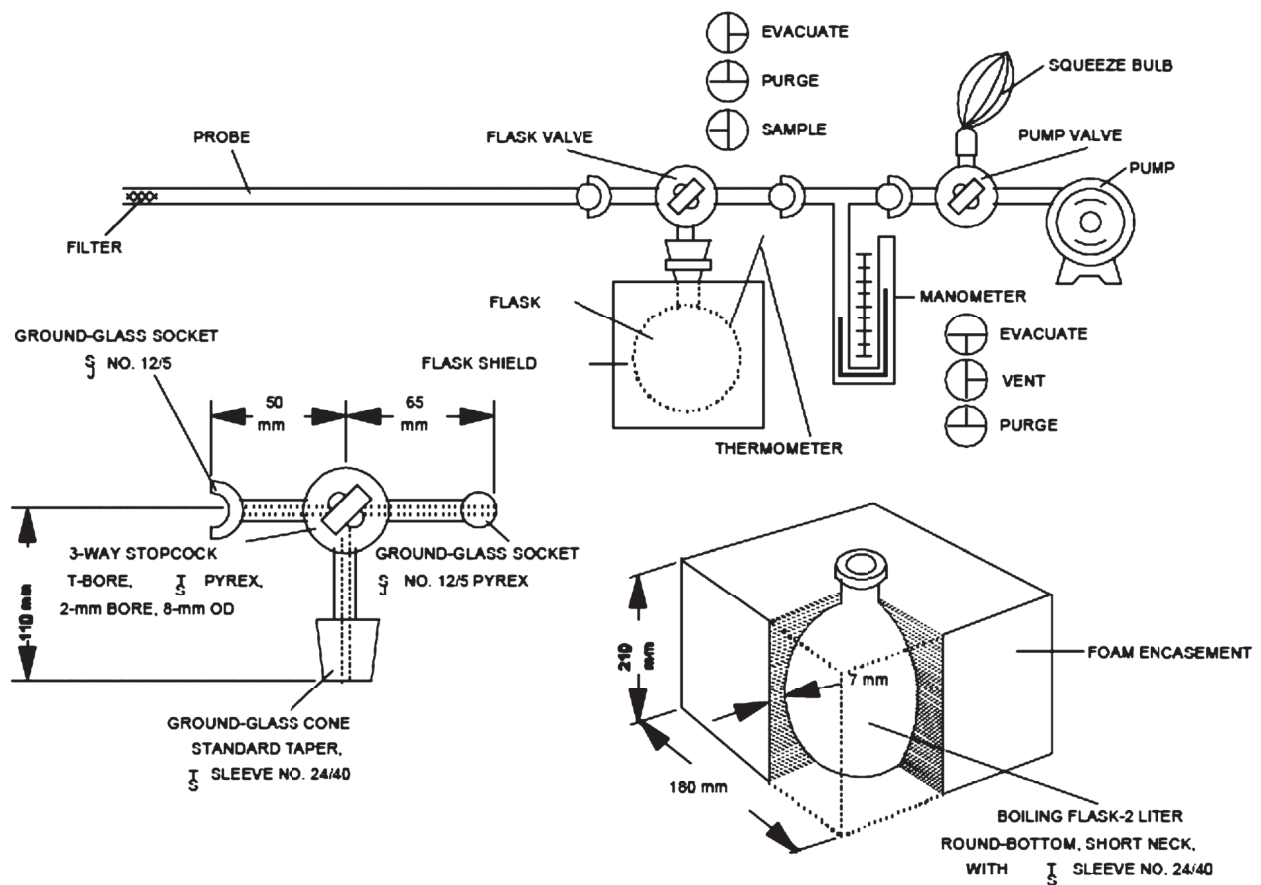


Figure 7-1. Sampling Train, Flask Valve, and Flask



### **2.3.2 Porcelain Evaporating Dishes**

175- to 250-ml capacity with lip for pouring, one for each sample and each standard.

### **2.3.3 Steam Bath**

Low-temperature ovens or thermostatically controlled hot plates kept below 70 °C (160 °F) are acceptable alternatives.

### **2.3.4 Dropping Pipette or Dropper**

Three required.

### **2.3.5 Polyethylene Policeman**

One for each sample and each standard.

### **2.3.6 Graduated Cylinder**

100-ml with 1-ml divisions.

### **2.3.7 Volumetric Flasks**

50-ml (one for each sample and each standard), 100-ml (one for each sample and each standard, and one for the working standard KNO<sub>3</sub> solution), and 1000-ml one).

### **2.3.8 Spectrophotometer**

To measure at 410 nm.

### **2.3.9 Graduated Pipette.**

10-ml with 0.1-ml divisions.

### **2.3.10 Test Paper for Indicating pH**

To cover the pH range of 7 to 14.

### **2.3.11 Analytical Balance**

To measure to within 0.1 mg.

## **3. REAGENTS**

Unless otherwise indicated, it is intended that all reagents conform to the specifications established by the Committee on Analytical Reagents of the American Chemical Society, where such specifications are available; otherwise, use the best available grade.

### **3.1 Sampling**

Two reagents are required:

#### **3.1.1 Water**

Deionized distilled to conform to ASTM specification D 1193—77, Type 3. At the option of the analyst, the KMnO<sub>4</sub> test for oxidizable organic matter may be omitted when high concentrations of organic matter are not expected to be present.

#### **3.1.2 Absorbing Solution**

Cautiously add 2.8 ml concentrated H<sub>2</sub>SO<sub>4</sub> to 1 liter of water. Mix well, and add 6 ml of 3 percent hydrogen peroxide, freshly prepared from 30 percent hydrogen peroxide solution. The absorbing solution should be used within 1 week of its preparation. Do not expose to extreme heat or direct sunlight.

### **3.2 Sample Recovery**

Two reagents are required for sample recovery:

#### **3.2.1 Water**

Same as in 3.1.1.

#### **3.2.2 Sodium Hydroxide, 1 N**

Dissolve 40 g NaOH in water, and dilute to 1 liter.

### **3.3 Analysis**

For the analysis, the following reagents are required:

#### **3.3.1 Water**

Same as in 3.1.1.

#### **3.3.2 Sulfuric Acid**

Concentrated, 95 percent minimum assay. HANDLE WITH CAUTION.

#### **3.3.3 Potassium Nitrate (KN03)**

Dried at 105 to 110 °C (220 to 230 °F) for a minimum of 2 hours just prior to preparation of standard solution.

#### **3.3.4 Standard KN03 Solution**

Dissolve exactly 2.198 g of dried KN03 in water, and dilute to 1 liter with water in a 1000-ml volumetric flask.

#### **3.3.5 Working Standard KN03 Solution**

Dilute 10 ml of the standard solution to 100 ml with water. One milliliter of the working standard solution is equivalent to 100 µg nitrogen dioxide (N02).

#### **3.3.6 Phenoldisulfonic Acid Solution**

Dissolve 25 g of pure white phenol solid in 150 ml concentrated sulfuric acid on a steam bath. Cool, add 25 ml fuming sulfuric acid (15 to 18 percent by weight free sulfur trioxide - HANDLE WITH CAUTION), and heat at 100 °C (212 °F) for 2 hours. Store in a dark, stoppered bottle.

#### **3.3.7 Concentrated Ammonium Hydroxide**

Analytical Reagent grade or higher

### 3.3.8 Quality Assurance Audit Samples

Nitrate samples prepared from CRM (KNO<sub>3</sub>) shall be processed in same manner to satisfy audit criteria.

## 4. PROCEDURES

### 4.1 Sampling.

- Pipette 25 ml of absorbing solution into a sample flask, retaining a sufficient quantity for use in preparing the calibration standards. Insert the flask valve stopper into the flask with the valve in the "purge" position. Assemble the sampling train as shown in Figure 7-1, and place the probe at the sampling point. Make sure that all fittings are tight and leak-free, and that all ground glass joints have been greased properly with a high-vacuum, high temperature chlorofluorocarbon-based stopcock grease. Turn the flask valve and the pump valve to their "evacuate" positions. Evacuate the flask to 75 mm (3 in.) Hg absolute pressure, or less. Evacuation to a pressure approaching the vapor pressure of water at the existing temperature is desirable. Turn the pump valve to its "vent" position, and turn off the pump. Check for leakage by observing the manometer for any pressure fluctuation. (Any variation greater than 10 mm (0.4 in.) Hg over a period of 1 minute is not acceptable, and the flask is not to be used until the leakage problem is corrected. Pressure in the flask is not to exceed 75 mm (3 in.) Hg absolute at the time sampling is commenced.) Record the volume of the flask and valve ( $V_f$ ), the flask temperature ( $T_i$ ), and the barometric pressure. Turn the flask valve counterclockwise to its "purge" position, and do the same with pump valve. Purge the probe and the vacuum tube using the squeeze bulb. If condensation occurs in the probe and the flask valve area, heat the probe, and purge until the condensation disappears. Next, turn the pump valve to its "vent" position. Turn the flask valve clockwise to its "evacuate" position, and record the difference in the mercury levels in the manometer. The absolute internal pressure in the flask ( $P_i$ ) is equal to the barometric pressure less the manometer reading. Immediately turn the flask valve to the "sample" position, and permit the gas to enter the flask until pressures in the flask and sample line (i.e., duct, stack) are equal. This will usually require about 15 seconds; a longer period indicates a "plug" in the probe, which must be corrected before sampling is continued. After collecting the sample, turn the flask valve to its "purge" position, and disconnect the flask from the sampling train. Shake the flask for at least 5 minutes.
- If the gas being sampled contains insufficient oxygen for the conversion of NO to NO<sub>2</sub> (e.g., an applicable subpart of the standard may require taking a sample of a calibration gas mixture of NO in N<sub>2</sub>), then introduce oxygen into the flask to permit this conversion. Oxygen may be introduced into the flask by one of three methods: (1) Before evacuating the sampling flask, flush with pure cylinder oxygen, then evacuate flask to 75 mm (3 in.) Hg absolute pressure or less; or (2) inject oxygen into the flask after sampling; or (3) terminate sampling with a minimum of 50 mm (2 in.) Hg vacuum remaining in the flask, record this final pressure, and then vent the flask to the atmosphere until the flask pressure is almost equal to atmospheric pressure.

## 4.2 Sample Recovery

Let the flask set for a minimum of 16 hours, and then shake the contents for 2 minutes. Connect the flask to a mercury filled U—tube manometer. Open the valve from the flask to the manometer, and record the flask temperature (Tf), the barometric pressure, and the difference between the mercury levels in the manometer. The absolute internal pressure in the flask (Pf) is the barometric pressure less the manometer reading. Transfer the contents of the flask to a leak-free polyethylene bottle. Rinse the flask twice with 5-ml portions of water, and add the rinse water to the bottle. Adjust the pH to between 9 and 12 by adding sodium hydroxide (1 N), dropwise (about 25 to 35 drops). Check the pH by dipping a stirring rod into the solution and then touching the rod to the pH test paper. Remove as little material as possible during this step. Mark the height of the liquid level so that the container can be checked for leakage after transport. Label the container to identify clearly its contents. Seal the container for shipping.

## 4.3 Analysis.

- Note the level of the liquid in the container, and confirm whether any sample was lost during shipment; note this on the analytical data sheet. If a noticeable amount of leakage has occurred, either void the sample or use methods, subject to the approval of the Administrator, to correct the final results.
- Immediately prior to analysis, transfer the contents of the shipping container to a 50-ml volumetric flask, and rinse the container twice with 5— ml portions of water. Add the rinse water to the flask, and dilute to mark with water; mix thoroughly. Pipette a 25-ml aliquot into the porcelain evaporating dish. Return any unused portion of the sample to the polyethylene storage bottle. Evaporate the 25-ml aliquot to dryness on a steam bath, and allow to cool. Add 2 ml phenoldisulfonic acid solution to the dried residue, and triturate thoroughly with a polyethylene policeman. Make sure the solution contacts all the residue. Add 1 ml water and 4 drops of concentrated sulfuric acid. Heat the solution on a steam bath for 3 minutes with occasional stirring. Allow the solution to cool, add 20 ml water, mix well by stirring, and add concentrated ammonium hydroxide, dropwise, with constant stirring, until the pH is 10 (as determined by pH paper). If the sample contains solids, these must be removed by filtration (centrifugation is an acceptable alternative), as follows: Filter through Whatman No. 41 filter paper into a 100-ml volumetric flask; rinse the evaporating dish with three 5-ml portions of water; filter these three rinses. Wash the filter with at least three 15-ml portions of water. Add the filter washings to the contents of the volumetric flask, and dilute to the mark with water. If solids are absent, the solution can be transferred directly to the 100-ml volumetric flask and diluted to the mark with water.
- Mix the contents of the flask thoroughly, and measure the absorbance at the optimum wavelength used for the standards (Section 5.2.1), using the blank solution as a zero reference. Dilute the sample and the blank with equal volumes of water if the absorbance exceeds A4, the absorbance of the 400- $\mu$ g N02 standard (see Section 5.2.2).

#### 4.4 Audit Sample Analysis.

- Concurrently analyze the two audit samples and a set of compliance samples (Section 4.3) in the same manner to evaluate the technique of the analyst and the standards preparation. (Note: It is recommended that known quality control samples be analyzed prior to the compliance and audit sample analysis to optimize the system accuracy and precision. One source of these samples is the Source Branch listed in Section 3.3.9.) The same analysts, analytical reagents.
- Calculate the concentrations in mg/dsm<sup>3</sup> (mg/NM<sup>3</sup>) using the specified sample volume in the audit instructions.
- The concentrations of the audit samples obtained by the analyst shall agree within 10 percent of the actual audit concentrations. If the 10—percent specification is not met, reanalyze the compliance samples and audit samples, and include initial and reanalysis values in the test report
- Failure to meet the 10-percent specification may require retests until the audit problems are resolved. However, if the audit results do not affect the compliance or noncompliance status of the affected facility, the Administrator may waive the reanalysis requirement, further audits, or retests and accept the results of the compliance test. While steps are being taken to resolve audit analysis problems,

### 5. CALIBRATION

**5.1 Flask Volume.** The volume of the collection flask-flask valve combination must be known prior to sampling. Assemble the flask and flask valve, and fill with water to the stopcock. Measure the volume of water to  $\pm 10$  ml. Record this volume on the flask.

#### 5.2 Spectrophotometer Calibration.

##### 5.2.1 Optimum Wavelength Determination.

- Calibrate the wavelength scale of the spectrophotometer every 6 months. The calibration may be accomplished by using an energy source with an intense line emission such as a mercury lamp, or by using a series of glass filters spanning the measuring range of the spectrophotometer. Calibration materials are available commercially and from the National Bureau of Standards. Specific details on the use of such materials should be supplied by the vendor; general information about calibration techniques can be obtained from general reference books on analytical chemistry. The wavelength scale of the spectrophotometer must read correctly within 5 nm at all calibration points; otherwise, repair and recalibrate the spectrophotometer. Once the wavelength scale of the spectrophotometer is in proper calibration, use 410 nm as the optimum wavelength for the measurement of the absorbance of the standards and samples.
- Alternatively, a scanning procedure may be employed to determine the proper measuring wavelength. If the instrument is a double-beam spectrophotometer, scan the spectrum

between 400 and 415 nm using a 200  $\mu\text{g}$   $\text{NO}_2$  standard solution in the sample cell and a blank solution in the reference cell. If a peak does not occur, the spectrophotometer is probably malfunctioning and should be repaired. When a peak is obtained within the 400 to 415 nm range, the wavelength at which this peak occurs shall be the optimum wavelength for the measurement of absorbance of both the standards and the samples. For a single beam spectrophotometer, follow the scanning procedure described above, except scan separately the blank and standard solutions. The optimum wavelength shall be the wavelength at which the maximum difference in absorbance between the standard and the blank occurs.

### 5.2.2 Determination of Spectrophotometer Calibration Factor $K_c$ .

Add 0.0 ml, 2.0 ml, 4.0 ml, 6.0 ml, and 8.0 ml of the  $\text{KNO}_3$  working standard solution (1 ml = 100  $\mu\text{g}$   $\text{NO}_2$ ) to a series of five 50-ml volumetric flasks. To each flask, add 25 ml of absorbing solution, 10 ml water, and sodium hydroxide (1 N) drop wise until the pH is between 9 and 12 (about 25 to 35 drops each). Dilute to the mark with water. Mix thoroughly, and pipette a 25-ml aliquot of each solution into a separate porcelain evaporating dish. Beginning with the evaporation step, follow the analysis procedure of Section 4.3 until the solution has been transferred to the 100-ml volumetric flask and diluted to the mark. Measure the absorbance of each solution, at the optimum wavelength, as determined in Section 5.2.1. This calibration procedure must be repeated on each day that samples are analyzed. Calculate the spectrophotometer calibration factor as follows:

$$K_c = 100 \frac{A_1 + 2A_2 + 3A_3 + 4A_4}{A_1^2 + A_2^2 + A_3^2 + A_4^2} \quad \text{Eq. 7-1}$$

Where:

$K_c$  = Calibration factor.

$A_1$  = Absorbance of the 100 -  $\mu\text{g}$   $\text{NO}_2$  Standard.

$A_2$  = Absorbance of the 200 -  $\mu\text{g}$   $\text{NO}_2$  Standard.

$A_3$  = Absorbance of the 300 -  $\mu\text{g}$   $\text{NO}_2$  Standard.

$A_4$  = Absorbance of the 400 -  $\mu\text{g}$   $\text{NO}_2$  Standard.

### 5.2.3 Spectrophotometer Calibration Quality Control

Multiply the absorbance value obtained for each standard by the  $K_c$  factor (least squares slope) to determine the distance each calibration point lies from the theoretical calibration line. These calculated concentration values should not differ from the actual concentrations (i.e., 100, 200, 300, and 400  $\mu\text{g}$   $\text{NO}_2$ ) by more than 7 percent for three of the four standards.

### 5.3 Barometer

Calibrate against a mercury barometer.

### 5.4 Temperature Gauge

Calibrate dial thermometers against mercury-in-glass thermometers.



## 5.5 Vacuum Gauge.

Calibrate mechanical gauges, if used, against a mercury manometer such as that specified in 2.1.6.

## 5.6 Analytical Balance. Calibrate against standard weights.

### 6. CALCULATIONS

Carry out the calculations, retaining at least one extra decimal figure beyond that of the acquired data. Round off figures after final calculations.

#### 6.1 Nomenclature

A = Absorbance of sample.

C = Concentration of NO<sub>x</sub> as N<sub>2</sub>O, dry basis, corrected to standard conditions, mg/dsm<sup>3</sup> (1b/dscf).

F = Dilution factor (i.e., 25/5, 25/10, etc., required only if sample dilution was needed to reduce the absorbance into the range of the calibration).

K<sub>c</sub> = Spectrophotometer calibration factor.

m = Mass of NO<sub>x</sub> as NO<sub>2</sub> in gas sample, μg.

P<sub>f</sub> = Final absolute pressure of flask, mm Hg (in. Hg).

P<sub>i</sub> = Initial absolute pressure of flask, mm Hg (in. Hg).

P<sub>std</sub> = Standard absolute pressure, 760 mm Hg (29.92 in. Hg).

T<sub>f</sub> = Final absolute temperature of flask, °K (°R)

T<sub>i</sub> = Initial absolute temperature, of flask, °K (°R).

T<sub>std</sub> = Standard absolute temperature, 293 °K (528 °R).

V<sub>sc</sub> = Sample volume at standard conditions (dry basis), ml.

V<sub>f</sub> = Volume of flask and valve, ml.

V<sub>a</sub> = Volume of absorbing solution, 25 ml.

2 = 50/25, the aliquot factor. (If other than a 25-ml aliquot was used for analysis, the corresponding factor must be substituted).

#### 6.2 Sample Volume, Dry Basis, Corrected to Standard Conditions

$$V_{sc} = (V_f - V_a) \frac{T_{std}}{P_{std}} \left[ \frac{P_f}{T_f} - \frac{P_i}{T_i} \right]$$

$$= K_i (V_f - 25) \left[ \frac{P_f}{T_f} - \frac{P_i}{T_i} \right]$$

Eq. 7-3

Where :

$$K_1 = 0.3858 \text{ }^\circ\text{K/mm Hg for metric units,}$$
$$= 17.64 \text{ }^\circ\text{R/in. Hg for English units.}$$

### 6.3 Total $\mu\text{g NO}_2$ per sample.

$$m = 2 K_c A F$$

Note: If other than 25-ml aliquot is used for analysis , the factor 2 must be replaced by a corresponding factor.

### 6.4 Sample concentration, Dry Basis, Corrected to Standard Conditions.

$$C = K_2 (m/V_{sc})$$

Eq. 7-4

Where:

$$K_2 = 10^3 \text{ (mg /m}^3\text{) / } (\mu\text{g /ml) for metric units,}$$
$$= 6.242 \times 10^{-5} \text{ (lb / scf) / } (\mu\text{g / ml) for English units.}$$

### 6.5 Relative Error (RE) for QA audit Samples, Percent.

$$\text{RE} = 100 (C_d - C_a) / C_a$$

Eq. 7-5

Where:

$C_d$  = Determined audit sample concentration, mg / dsm<sup>3</sup>.

$C_a$  = Actual audit sample concentration, mg / dsm<sup>3</sup>.

## 7.0 BIBLIOGRAPHY

1. Standard Methods of Chemical Analysis. 6th ed. New York, D. Van Nostrand Co., Inc. 1962. Vol. 1, p. 329-330.
2. Standard Method of Test for Oxides of Nitrogen in Gaseous Combustion Products (Phenoldisulfonic Acid Procedure). In: 1968 Book of ASTM Standards, Part 26. Philadelphia, PA. 1968. ASTM Designation D 1608—60, p. 725-729.
3. Jacob, M.B. The Chemical Analysis of Air Pollutants. New York. Interscience Publishers, Inc. 1960. Vol. 10, p. 351-356.
4. Beatty, R.L., L.B. Berger, and H.H. Schrenk. Determination of Oxides of Nitrogen by the Phenoldisulfonic Acid Method. Bureau of Mines, U.S. Dept. of Interior. R.I. 3687. February 1943.
5. Hamil, H.F. and D.E. Camann. Collaborative Study of Method for the Determination of Nitrogen Oxide Emissions from Stationary Sources (Fossil Fuel-Fired Steam Generators). Southwest Research Institute Report for Environmental Protection Agency. Research Triangle Park, NC. October 5, 1973.
6. Hamil, H.F. and R.E. Thomas. Collaborative Study of Method for the determination of Nitrogen Oxide Emissions from Stationary Sources (Nitric Acid Plants). Southwest Research Institute Report for Environmental Protection Agency. Research Triangle Park, NC. May 8, 1974.



## CPCB brings out Reports under the following series:

|     |   |
|-----|---|
| 01. | Control of Urban Pollution Series (CUPS)  |
| 02. | Programme Objective Series (PROBES)   |
| 03. | Comprehensive Industry Document Series (COINDS)                                     |
| 04. | Assessment and Development Study of River Basin Series (ADSORBS)                    |
| 05. | Coastal Pollution Control Series (COPOCS)   |
| 06. | Laboratory Analytical Techniques Series (LATS)                                      |
| 07. | Monitoring of Indian National Aquatic Resources Series (MINARS)                     |
| 08. | National Ambient Air Quality Monitoring Series (NAAQMS)                             |
| 09. | Ecological Impact Assessment Series (EIAS)  |
| 10. | Pollution Control Law Series (PCLS)   |
| 11. | Hazardous Waste Management Series (HAZWAMS)   |
| 12. | Resource Recycling Series (RERES)   |
| 13. | Ground Water Quality Series (GWQS)  |
| 14. | Information Manual on Pollution Abatement and Cleaner Technologies Series (IMPACTS) |
| 15. | Environmental Mapping and Planning Series (EMAPS)                                   |
| 16. | Trace Organic Series (TOS)  |



**PARIVESH BHAWAN, CPCB HEAD OFFICE**

## Zonal Office of Central Pollution Control Board

### **BANGALORE**

1<sup>st</sup> and 2<sup>nd</sup> Floor, Nisarga Bhawan  
A-Block, Thimmaith Main Road, 7<sup>th</sup> D Cross,  
Shivanagar, Opp. Pushpanjali Theatre,  
Bangalore-560 010  
Tel. 080-23233827 (O) 080-23233739/  
23233827/23233996 Fax-080-23234059

### **BHOPAL**

3<sup>rd</sup> Floor, Shakar Bhawan,  
North TT Nagar  
Bhopal-462 003  
Tel. 0755-2775587 (O) 2775385/86  
(EPABX)  
Fax-0755-2775587

### **KOLKATA**

Southern Conclave  
Block 502, 5<sup>th</sup> & 6<sup>th</sup> Floor  
582 Rajdanga, Main Road,  
Kolkata-700 017  
Tel. 033-24416332 (Direct 24414289/  
4677/6003/6634 Fax-033-24418725

### **LUCKNOW**

Ground Floor, PICUP Bhawan,  
Vibhuti Khand, Gomti Nagar,  
Lucknow-226 010  
Tel. 0522-408760/2721915/16  
055-4087600 (EPABX)  
Fax-0522-2721891

### **SHILONG**

TUM-SIR Lower Motnagar,  
Near Fire Brigade H.Q.  
Shilong-793 014  
Tel. 0364-2520923/2522859  
Fax-0364-2520805

### **VADODARA**

Parivesh Bhawan  
Opp. VMC Ward Office No. 10,  
Subhanpura, Vadodara-390 023  
Tel. 0265-2283226/2283245  
Fax-0265-2283294

### **AGRA PROJECT OFFICE**

4, Dholpur House  
M.G. Road,  
Agra-282 001  
Tel. 0562-2421548  
Fax-0562-2421568

## **Central Pollution Control Board**

'Parivesh Bhawan, East Arjun Nagar  
Shahdara, Delhi-110 032  
Tel. 011-43102030  
Telefax-22305793/22307078/22301932/22304948  
Web: [cpcb.nic.in](http://cpcb.nic.in)